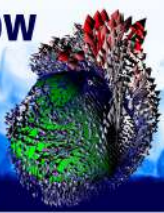


XIVth Multiphase Workshop and Summer School

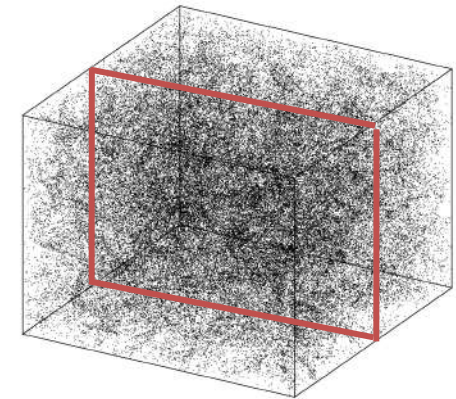
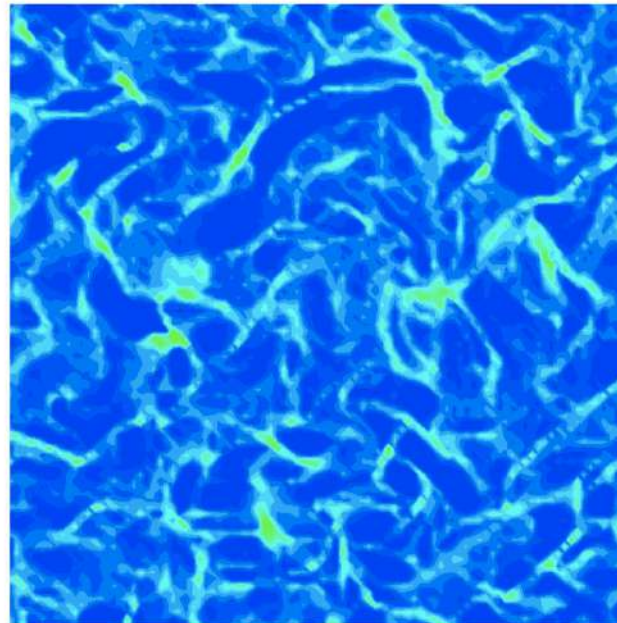


Point-particle simulations of complex turbulent dispersed flows

Cristian Marchioli
University of Udine & CISM



What's common to (almost) all particle-laden turbulent flows?

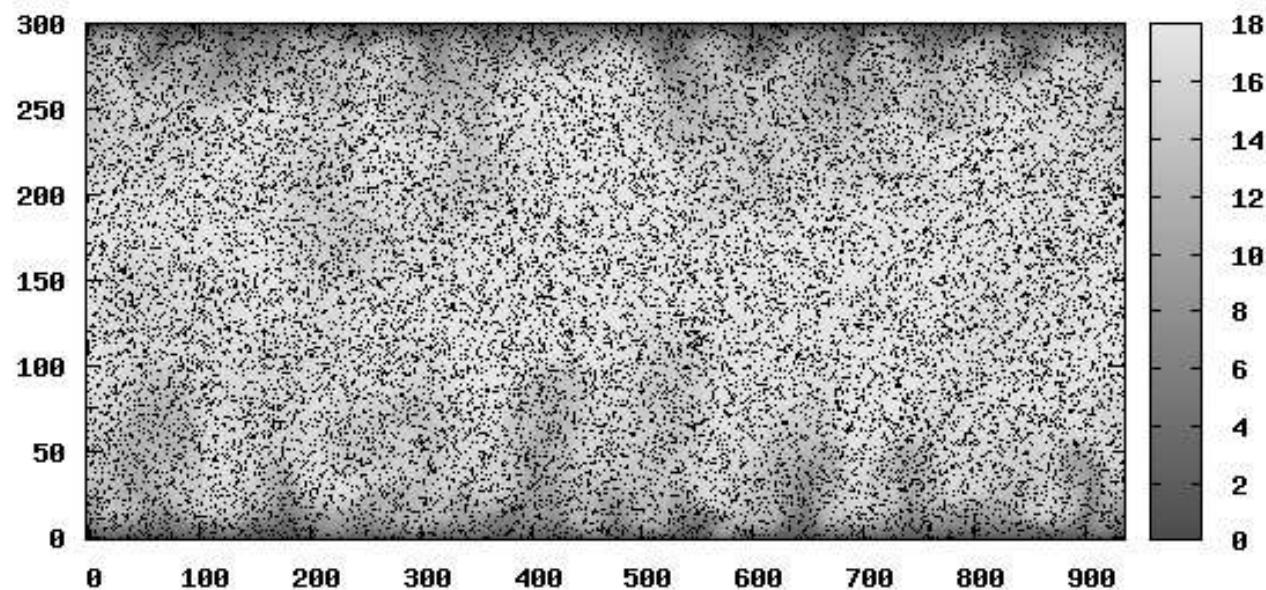
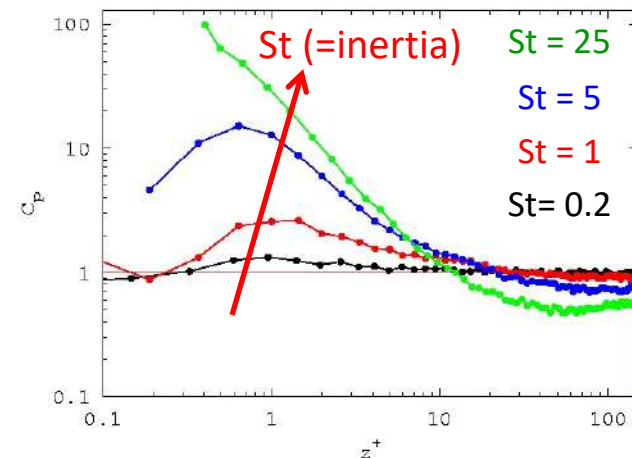
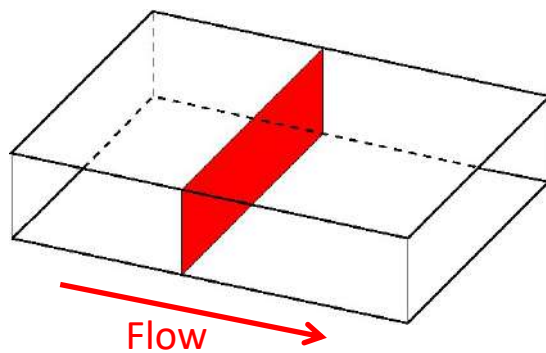


Particle number density in homogeneous isotropic turbulence ($Re_\lambda=51$, $St=1$)

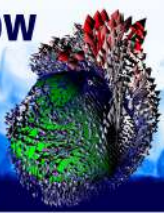
Particles concentrate preferentially in high-strain, low-vorticity regions due to their inertia

What's common to (almost) all particle-laden turbulent flows?

In wall-bounded flows inertial particles concentrate preferentially but also accumulate at the wall

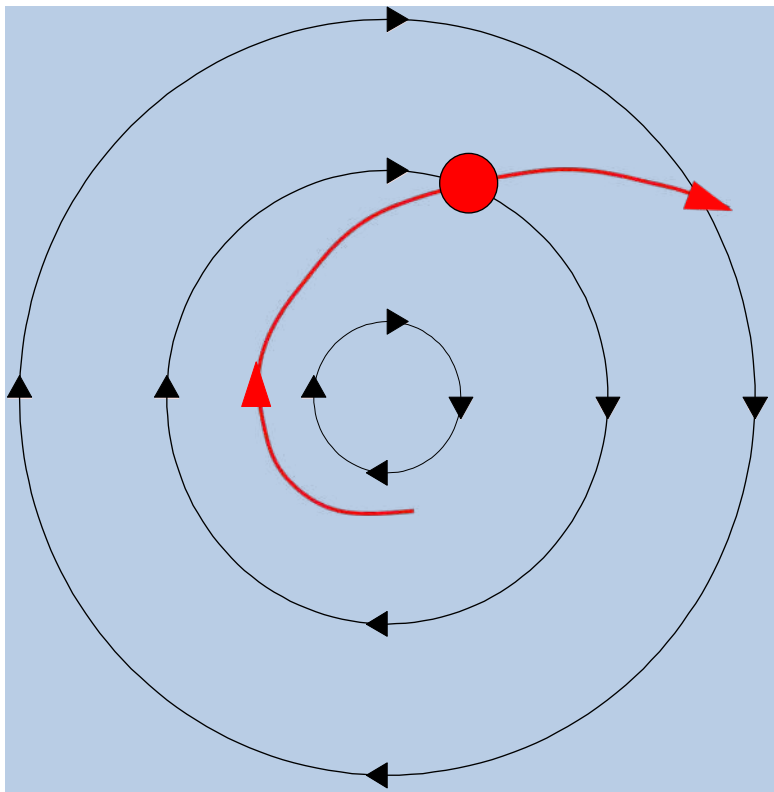


Time evolution of particle distribution
in a turbulent channel ($Re_\tau=150$, $St=25$)



What's common to (almost) all particle-laden turbulent flows?

My answer is: in all flows, particles tend to deviate from fluid streamlines!



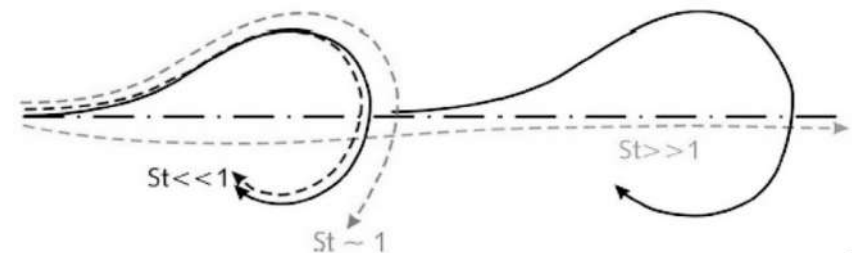
Only source of bias: particle inertia!

Deviations depend on the particle response time to the underlying flow field:

Particle Relaxation Time: $\tau_p = \frac{\rho_p d_p^2}{18\mu}$

Flow Time Scale: τ_f

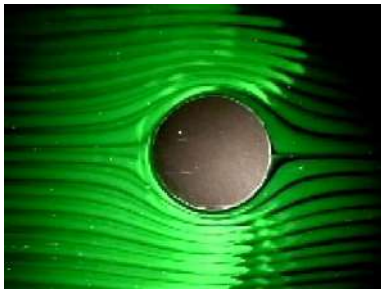
Particle Stokes number: $St = \frac{\tau_p}{\tau_f}$



A numerical approach to study preferential concentration

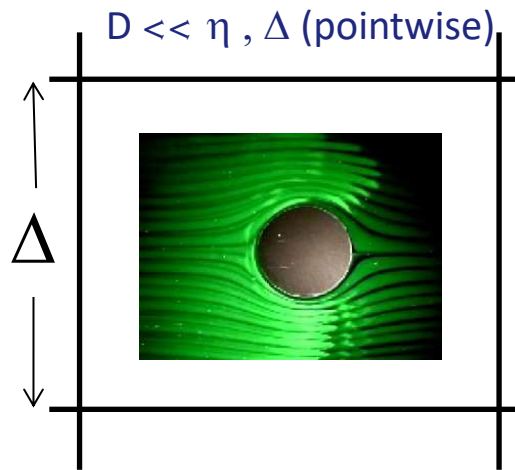
The simplest dynamical model to study “inertia-driven” preferential concentration considers small **pointwise** spherical particles (only source of bias is inertia!)

No wake (Stokes flow)



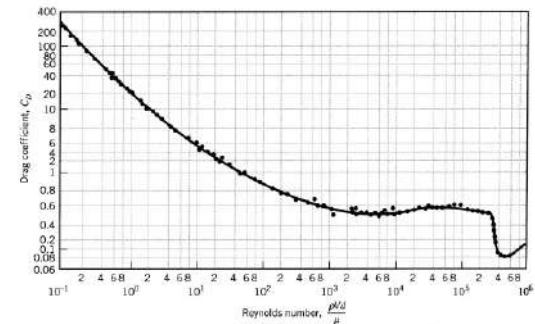
$$\text{Re}_p = \frac{u_{\text{rel}} L}{\nu} \ll 1$$

Enough to know
 \mathbf{x}_p and \mathbf{v}_p !



$$\frac{d\mathbf{x}_p}{dt} = \mathbf{v}_p, \quad m_p \frac{d\mathbf{v}_p}{dt} = \sum_i \mathbf{F}_i$$

Force model: Drag

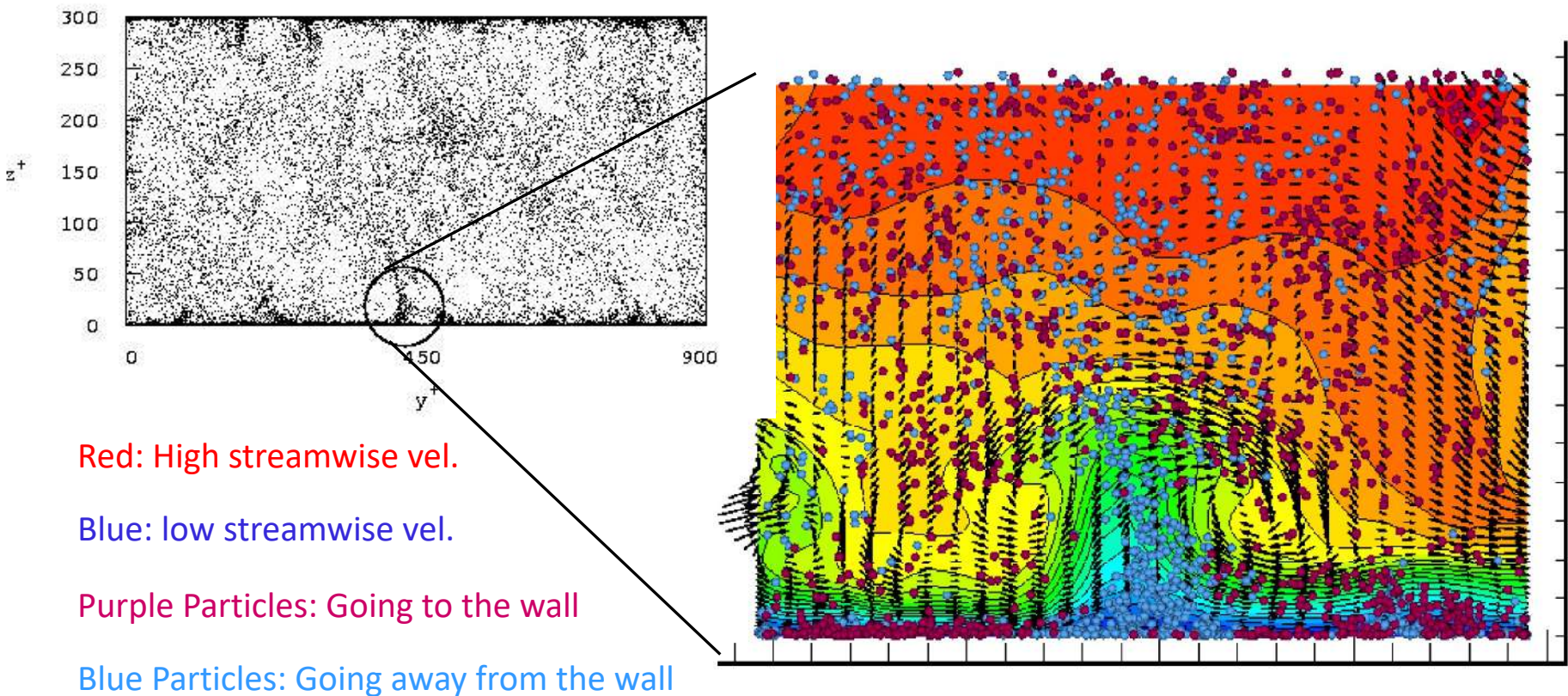


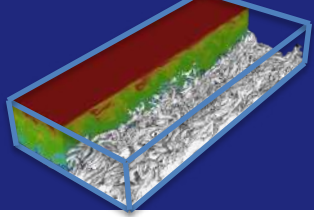
$$C_D(\text{Re}_p) = \frac{\mathbf{F}_D}{\frac{1}{2} \rho \mathbf{u}_{\text{rel}}^2 A_p}$$

Phenomenology of preferential concentration

Physics learned from this simple model (in DNS):

Qualitative explanation of particle deposition and entrainment in turbulent boundary layers



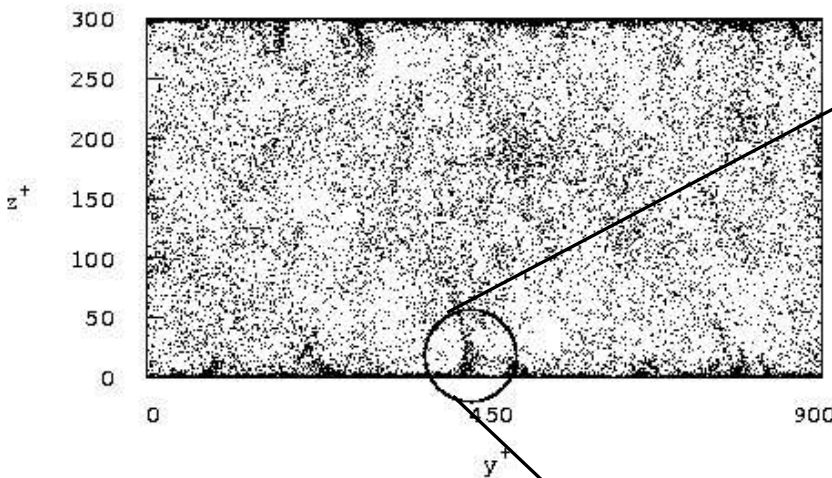


Phenomenology of preferential concentration

Physics learned from this simple model (in DNS):

Qualitative explanation of particle deposition and entrainment in turbulent boundary layers

STRUCTURES → SEGREGATION → ACCUMULATION → DEPOSITION

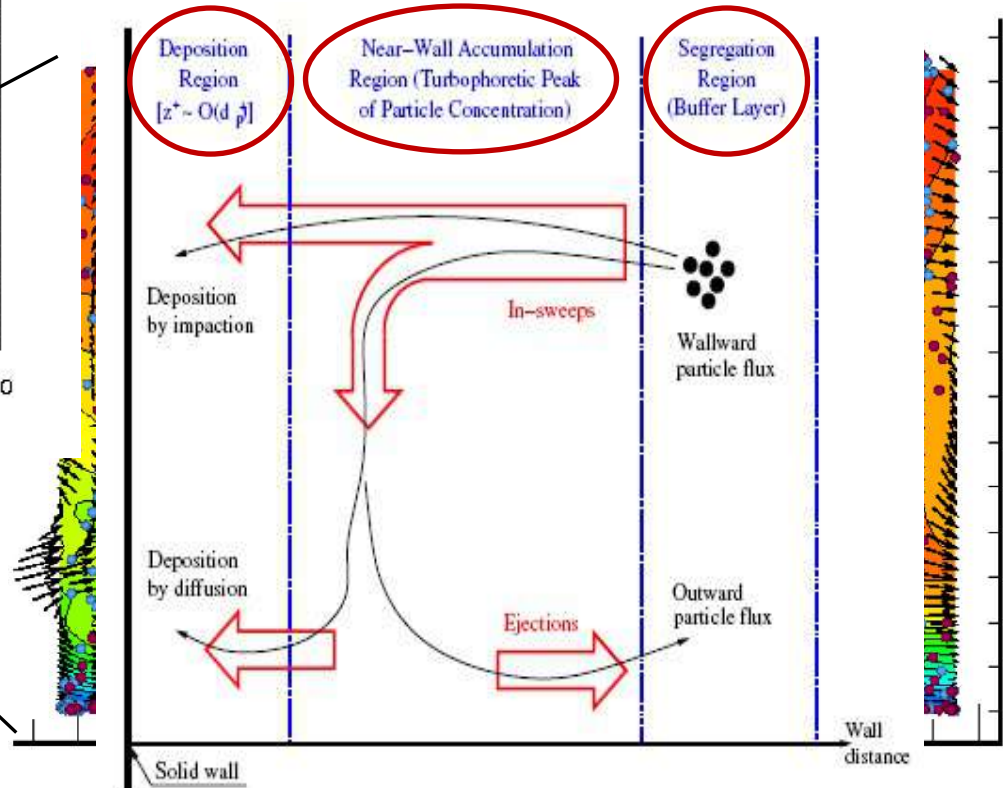


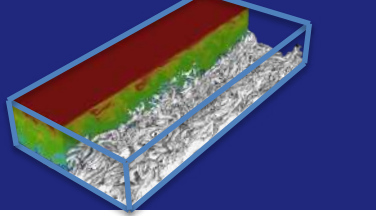
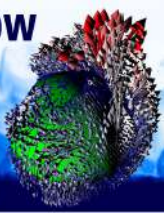
Red: High streamwise vel.

Blue: low streamwise vel.

Purple Particles: Going to the wall

Blue Particles: Going away from the wall



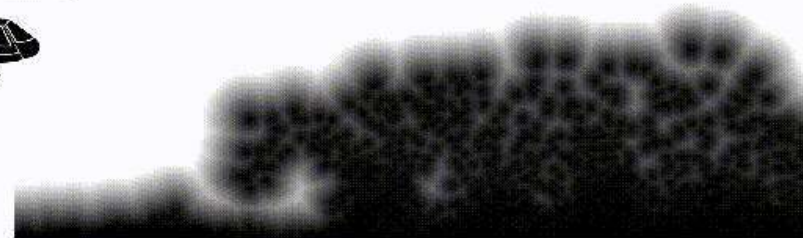


An interesting application: Rotor-wing brownout

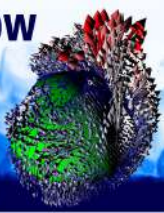


Figure courtesy of Chinook landing in the desert. Retrieved 27 Oct., 2014, from <http://www.defencetalk.com/dod-budget-cuts-stall-new-purchases-of-helicopters-44481/>

During brownout sand and dust are
resuspended from arid soil



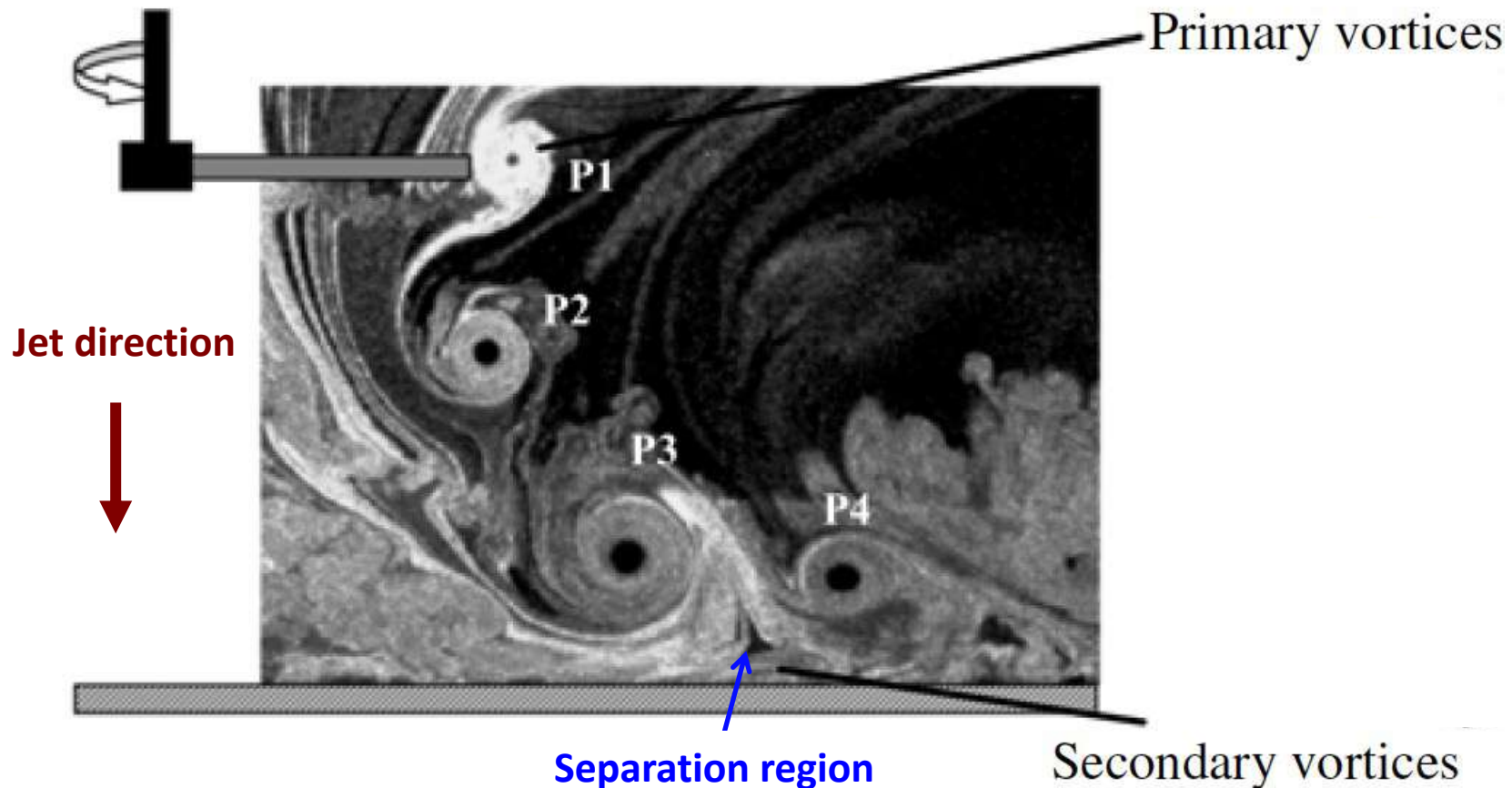
The downflow generated by the rotor-wing can be modelled as a
periodically-forced turbulent jet impinging on a solid wall

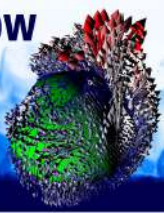


Resuspension by periodically-forced turbulent impinging jet

Flow field: Forced round imping jet

(cfr. Wu & Piomelli, JoT 2014 2016, EJM-B/Fluid 2015)

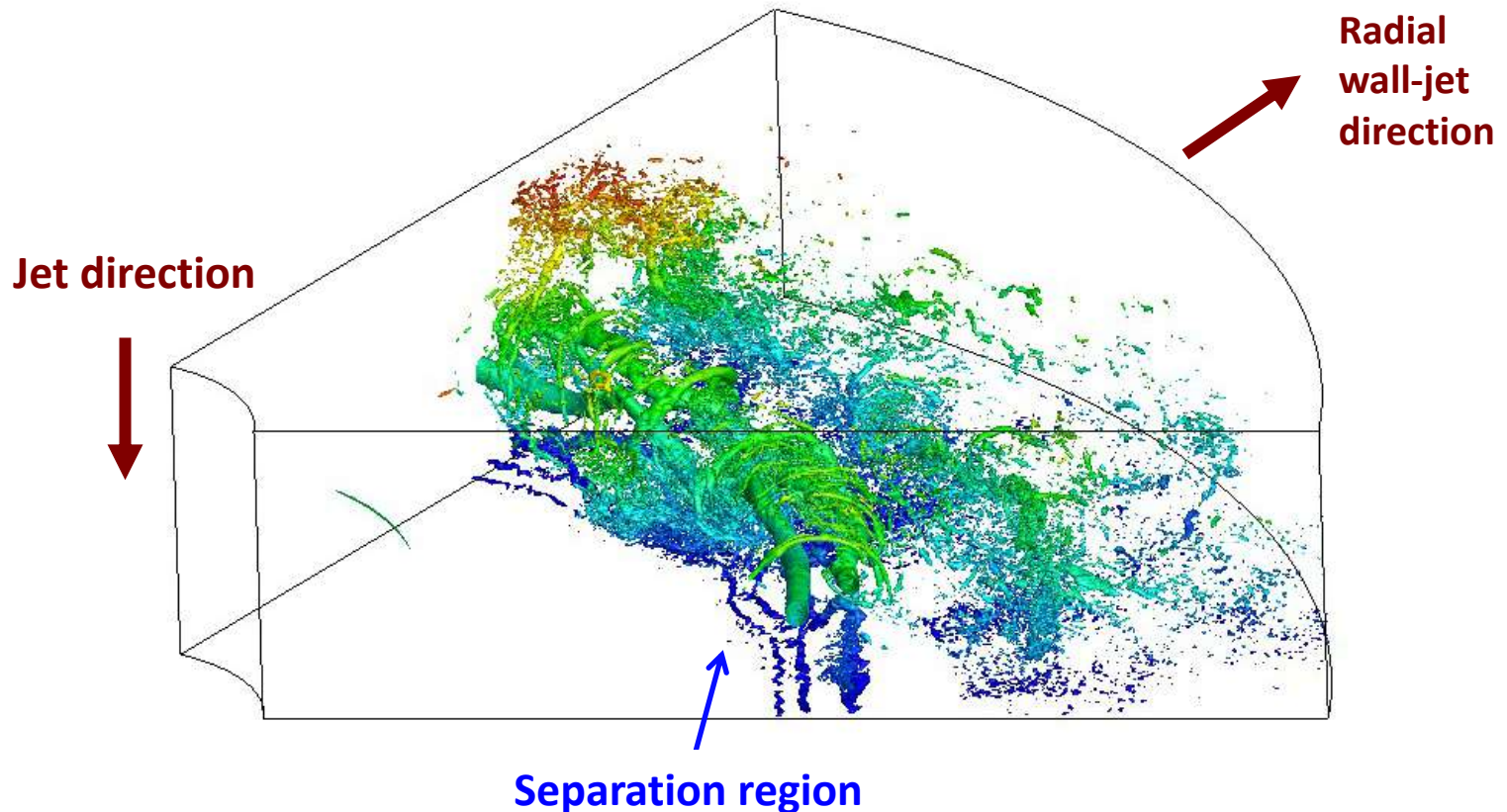


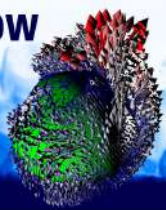


Resuspension by periodically-forced turbulent impinging jet

Flow field: Forced round imping jet

(cfr. Wu & Piomelli, JoT 2014 2016, EJM-B/Fluid 2015)





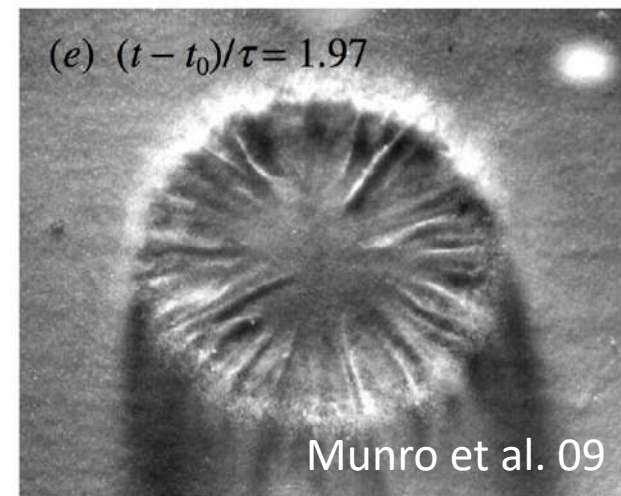
Resuspension by periodically-forced turbulent impinging jet

Question: What are the mechanisms governing particle resuspension ?

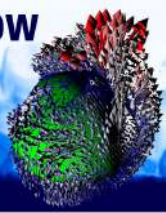
(cfr. Wu et al., JFM 2017)

Any analogy with sediment bed erosion by vortex rings?

(cfr. Munro et al., 2009; Bethke & Dalziel, 2012; Mulinti & Kiger, 2012; ...)



“Spokelike” scar features formed on the crater



Methodology

- Fluid

- Filtered continuity and Navier-Stokes equations

$$\nabla \cdot \bar{\mathbf{u}} = 0,$$

$$\frac{\partial \bar{\mathbf{u}}}{\partial t} + \nabla \cdot \bar{\mathbf{u}} \bar{\mathbf{u}} = -\nabla \bar{P} - \nabla \cdot \boldsymbol{\tau} + \nu_f \nabla^2 \bar{\mathbf{u}},$$

- 2nd-order accurate in space & time, staggered FD
- Lagrangian-averaged dynamic eddy-viscosity model

$$\frac{d\theta_p}{dt} = \frac{v_{p,\theta}}{r},$$

$$\frac{dr_p}{dt} = v_{p,r},$$

$$\frac{dz_p}{dt} = v_{p,z},$$

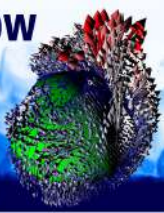
- Particles

- Lagrangian tracking
- Point-particle approach
- One-way coupling
- Forces: Drag, lift, buoyancy, gravity

$$\frac{dv_{p,\theta}}{dt} = \frac{C_D}{\tau_p} (\bar{u}_{@p,\theta} - v_{p,\theta}) - \frac{v_{p,\theta} v_{p,r}}{r} + f_{S,\theta},$$

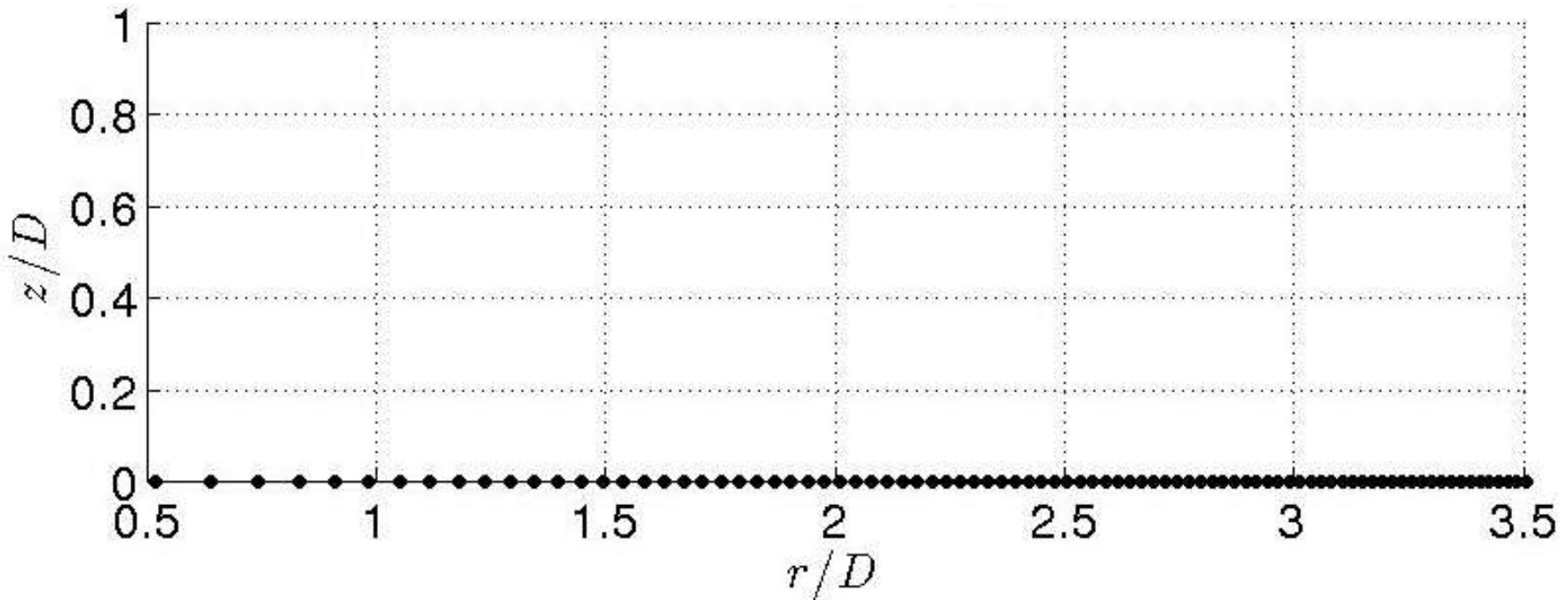
$$\frac{dv_{p,r}}{dt} = \frac{C_D}{\tau_p} (\bar{u}_{@p,r} - v_{p,r}) + \frac{v_{p,\theta}^2}{r} + f_{S,r},$$

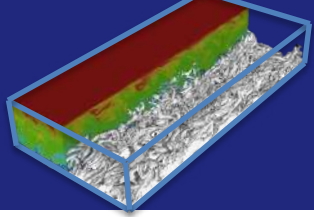
$$\frac{dv_{p,z}}{dt} = \frac{C_D}{\tau_p} (\bar{u}_{@p,z} - v_{p,z}) + \left(1 - \frac{\rho_f}{\rho_p}\right) g + f_{S,z},$$



Jet-induced particle resuspension

- Particle parameters
 - 20 micron; 50000 particles used; re-seed from inlet when exits





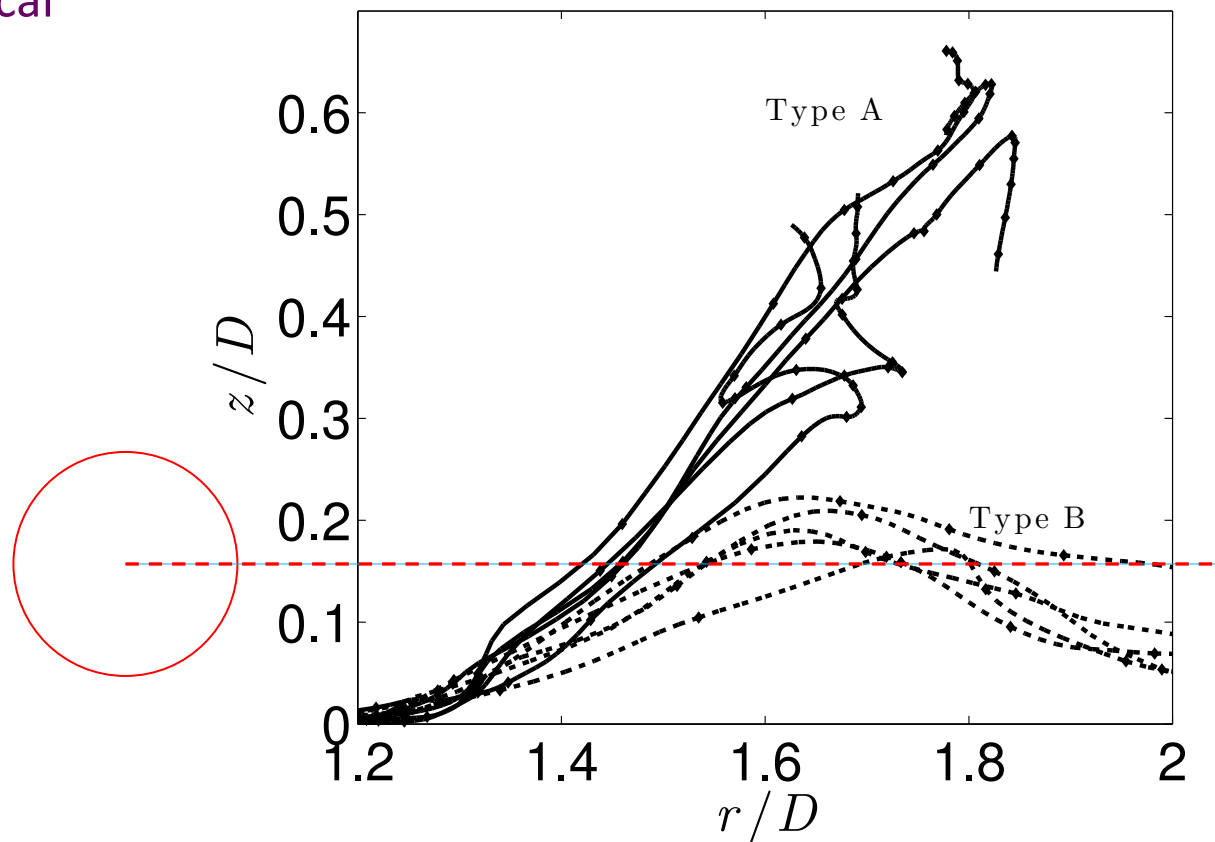
Jet-induced particle resuspension

- Different behaviors for identical particles
 - Must be caused by local flow characteristics

Type A: particles that reach $0.3D$ and higher

Type B: particles that stay below $0.3D$

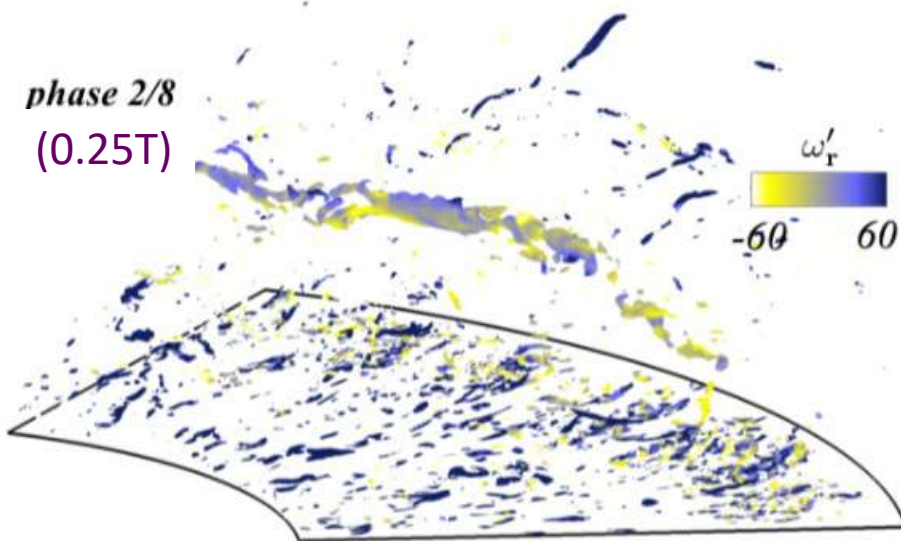
- Type B particles perform a small initial jump



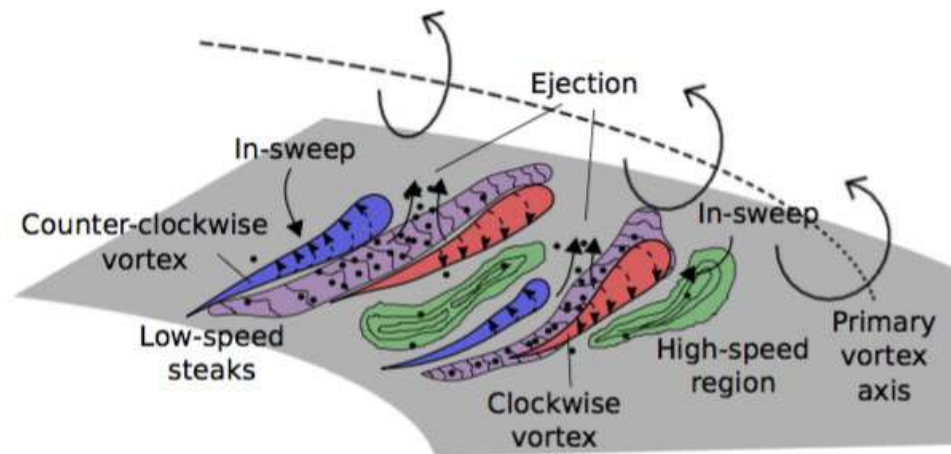
Jet-induced particle resuspension

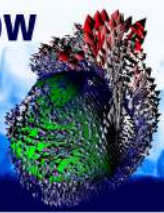
- Different behaviors for identical particles
 - Local flow characteristics: rib-like vortices, streaks, sweeps and ejections are observed in-between primary vortices

$$Q = (\Omega_{ij}\Omega_{ij} - S_{ij}S_{ij})/2$$



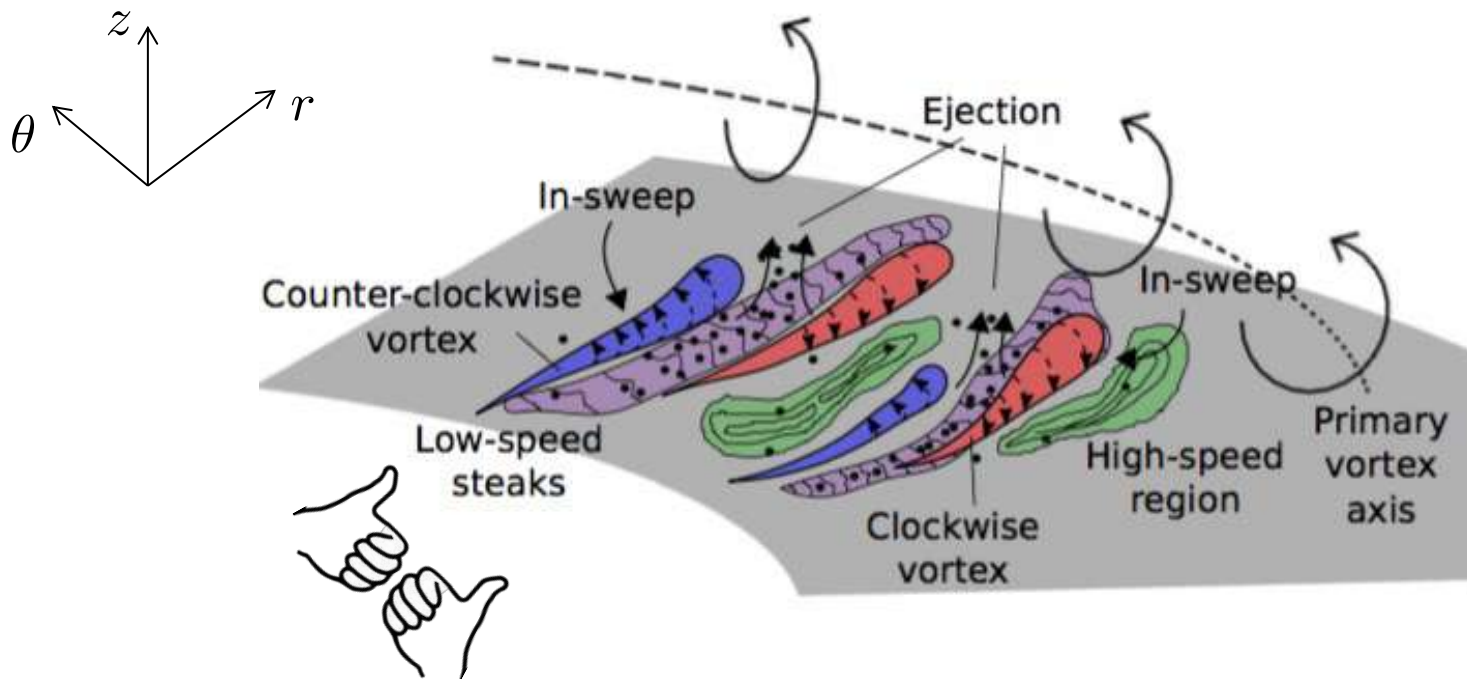
T = forcing period

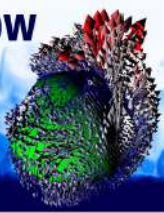




Jet-induced particle resuspension

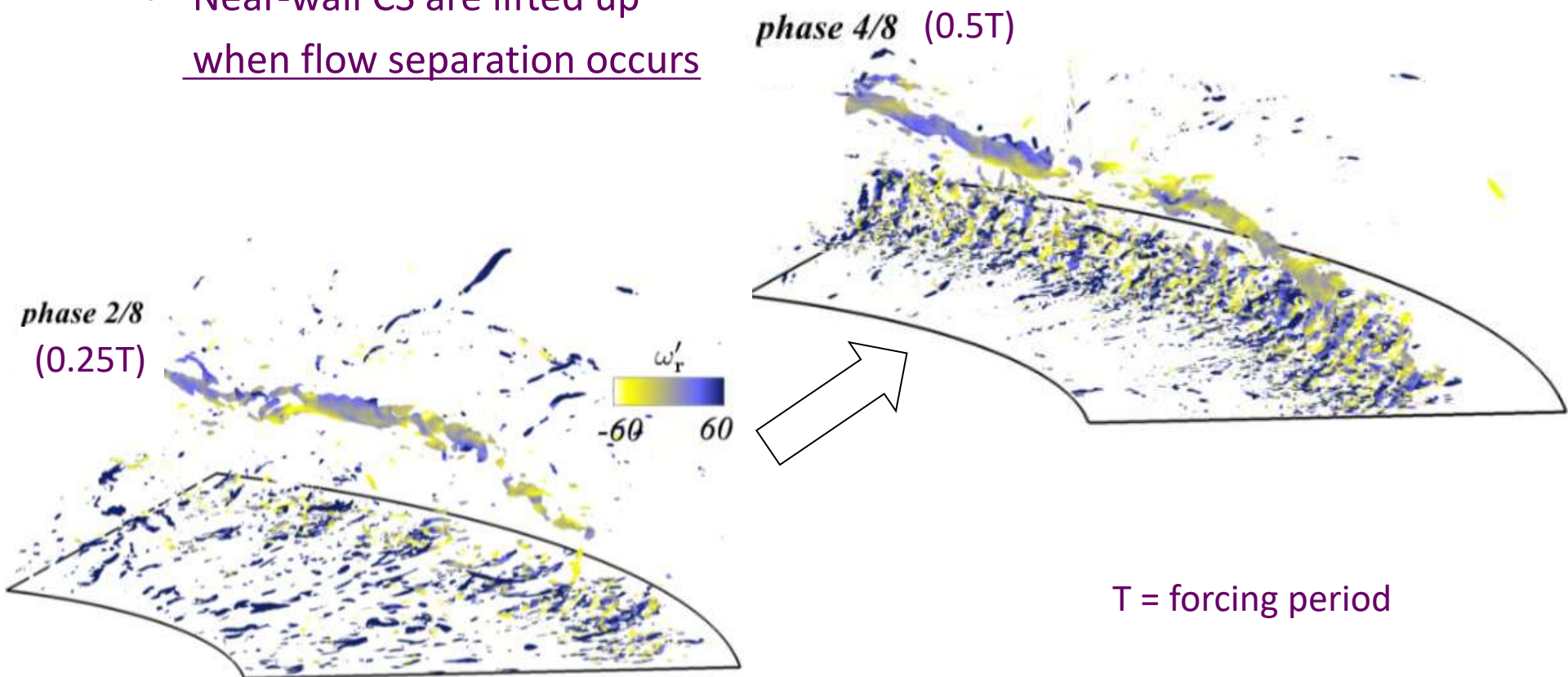
- Different behaviors for identical particles
 - Particles can be entrained by ejections (where $u'_{r,f} < 0$, $u'_{z,f} > 0$)





Jet-induced particle resuspension

- Different behaviors for identical particles
 - Near-wall CS are lifted up
when flow separation occurs

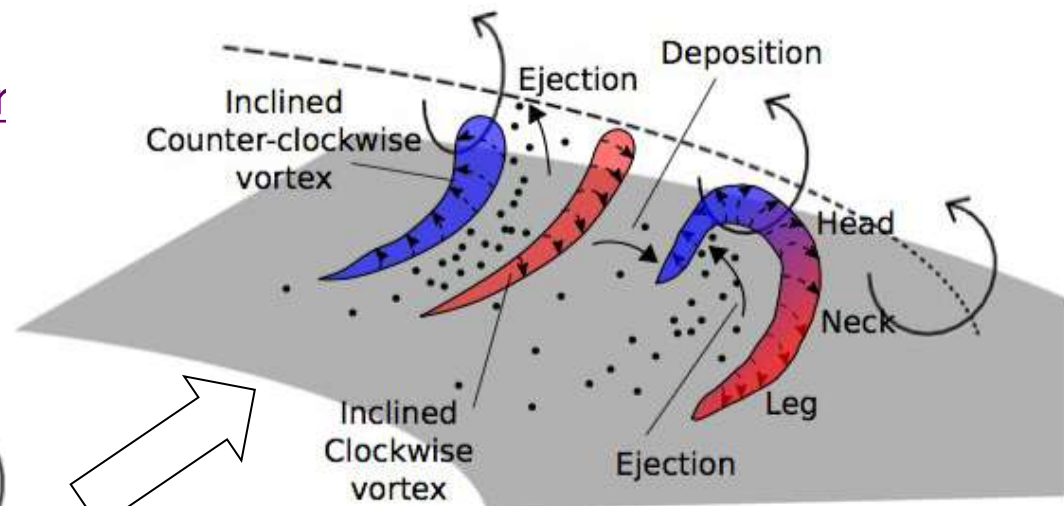
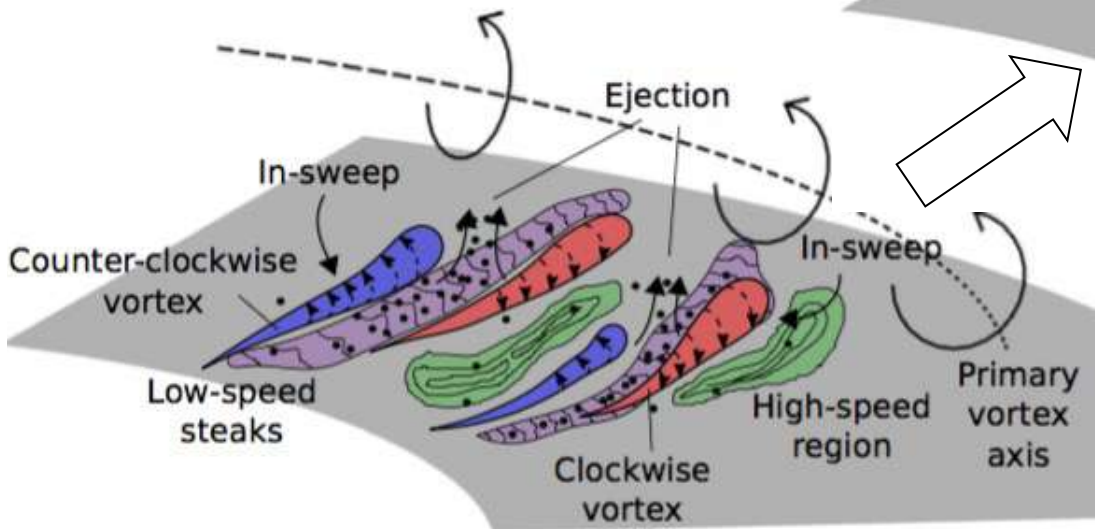


Jet-induced particle resuspension

- Different behaviors for identical particles
 - Near-wall CS are lifted up when flow separation occur

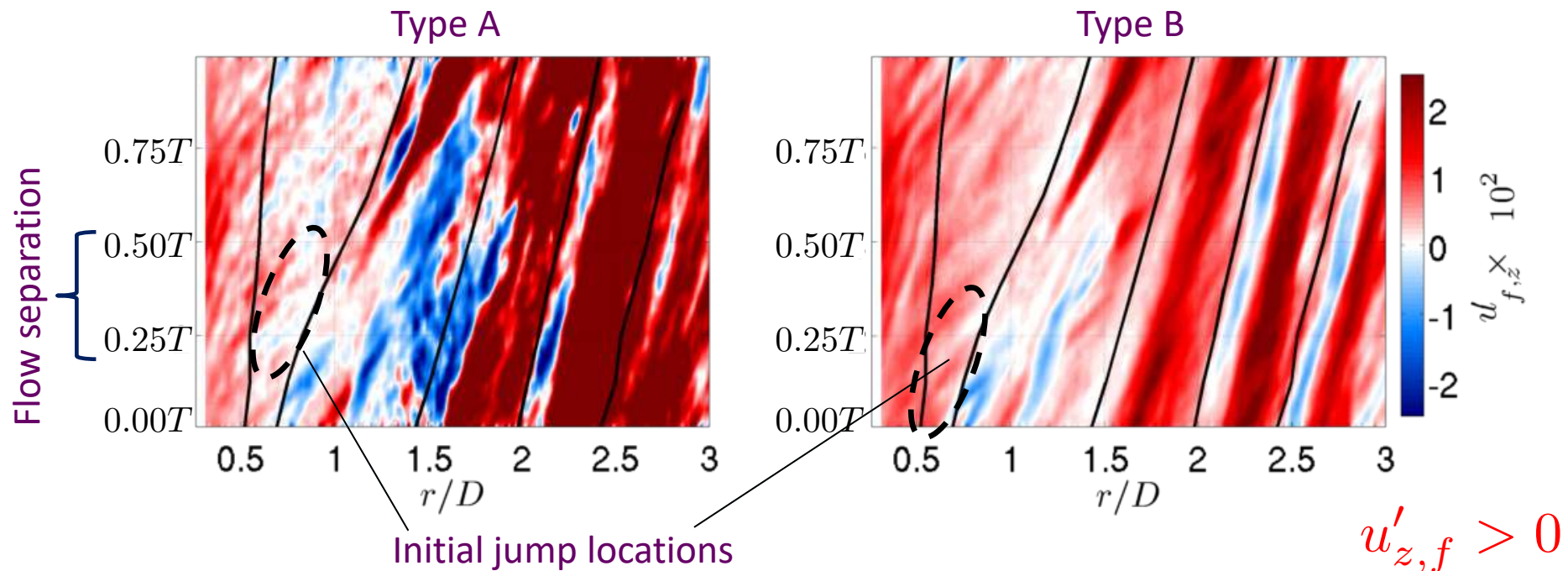
$$u'_{r,f} < 0$$

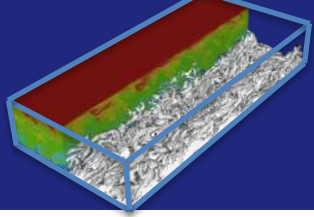
$$u'_{z,f} > 0$$



Jet-induced particle resuspension

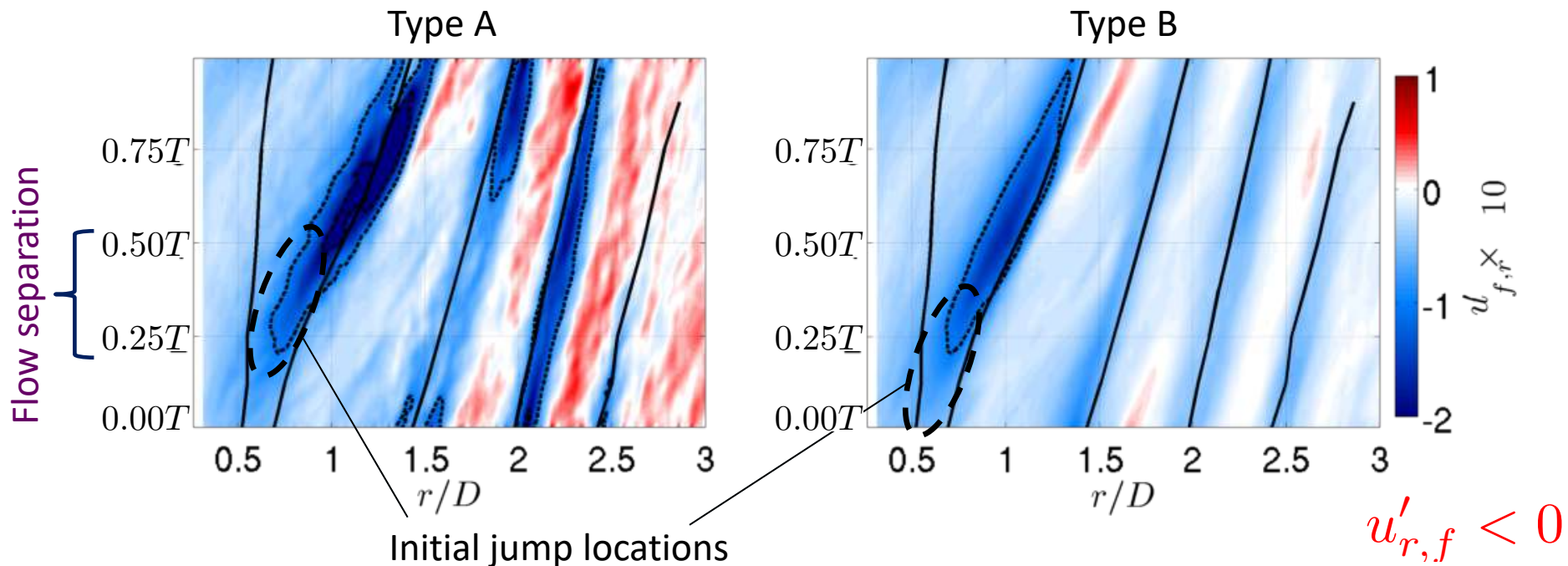
- Different behaviors for identical particles
 - Ejection by near-wall streaks
 - Type B particles: meet the right vortices, but at a wrong time

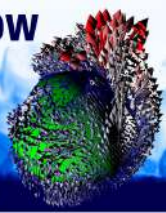




Jet-induced particle resuspension

- Different behaviors for identical particles
 - Ejection by near-wall streaks
 - Type B particles: meet the right vortices, but at a wrong time
 - Jump earlier, but streaks cannot sustain continuous ejection yet





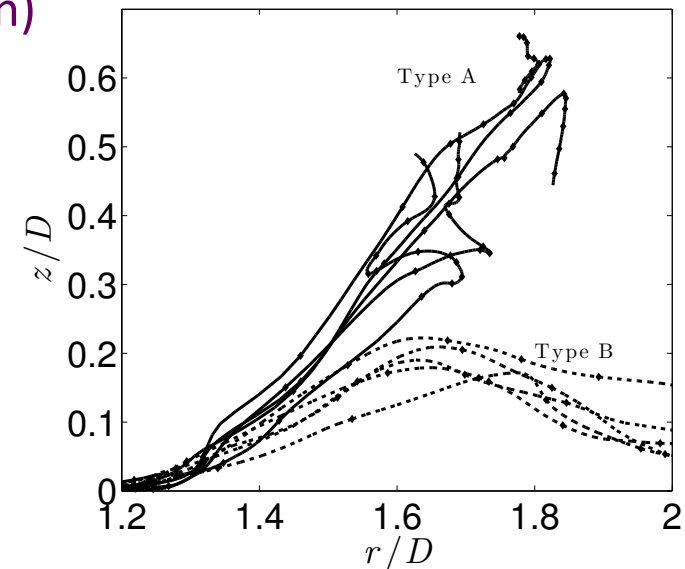
Jet-induced particle resuspension

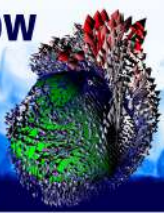
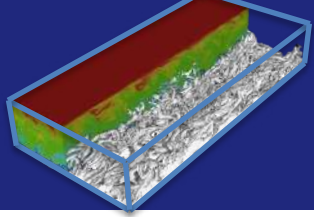
- Different behaviors for identical particles
 - **Mechanism 1:** in order to be continuously ejected in the near-wall region, a particle must
 1. meet the “right” streaks (the low-speed ones)
 2. at the “right” time (when the streaks are strong enough, namely near the separation region)



Jet-induced particle resuspension

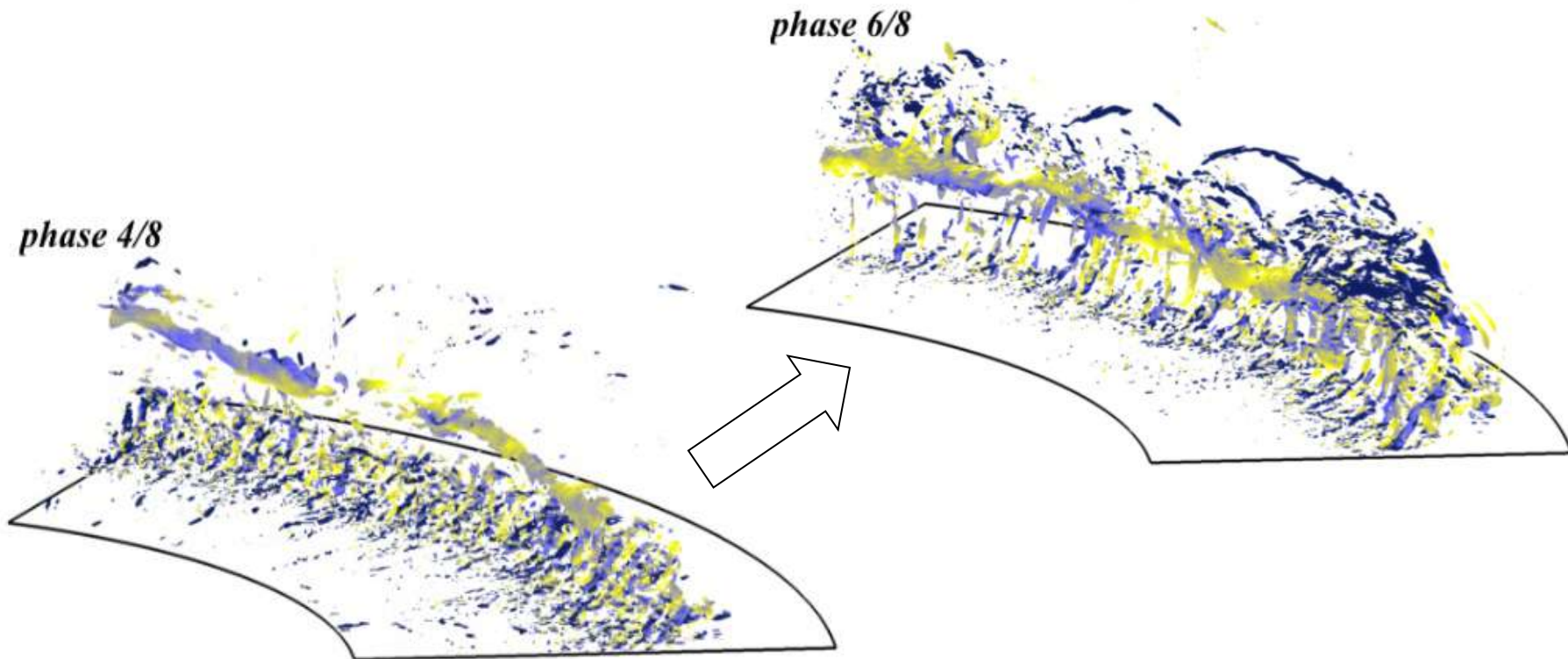
- Different behaviors for identical particles
 - **Mechanism 1:** in order to be continuously ejected in the near-wall region, a particle must
 1. meet the “right” streaks (the low-speed ones)
 2. at the “right” time (when the streaks are strong enough, namely near the separation region)
- Further question: how do particles get re-entrained far away from the wall and remain airborne?

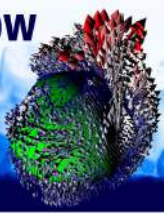




Jet-induced particle resuspension

- Lift-off of flow CS

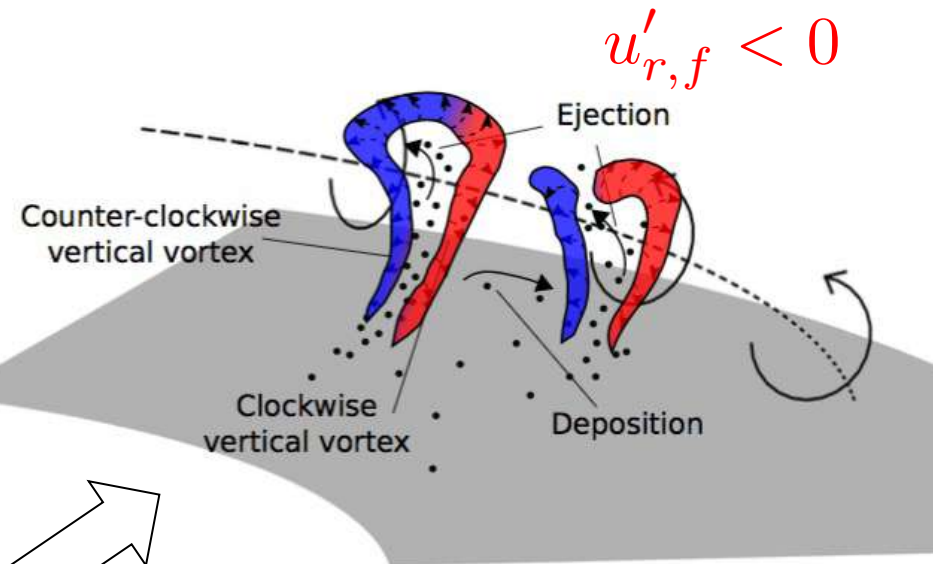
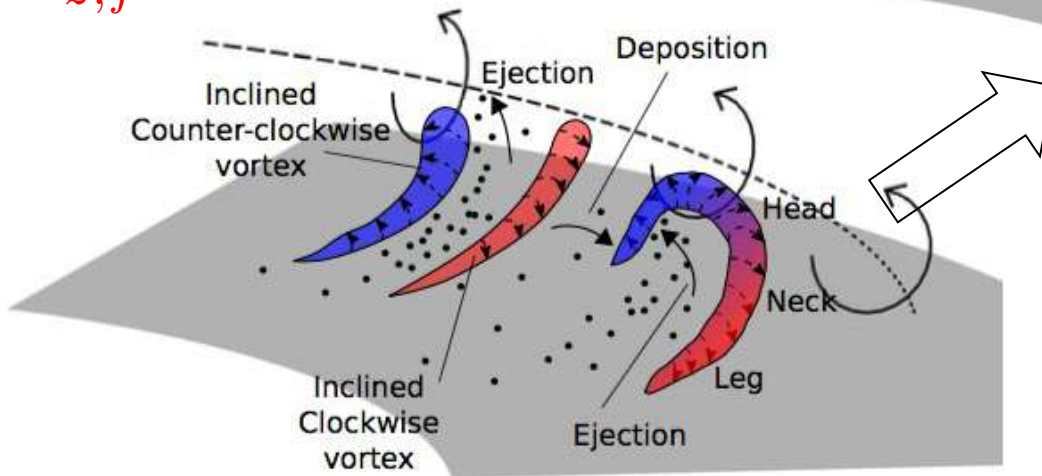




Jet-induced particle resuspension

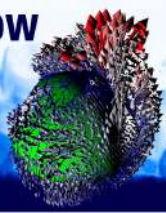
- Lift-off of flow CS

$$u'_{z,f} > 0$$



$$u'_{r,f} < 0$$

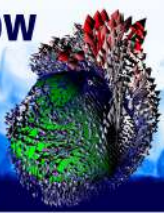
“Fence” effect of the vertical portion of the rib-like vortices



Jet-induced particle resuspension

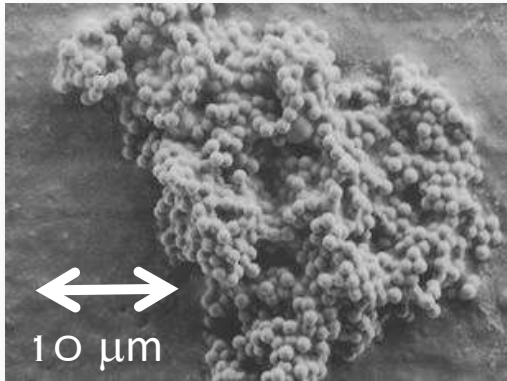
- Different behaviors for identical particles
 - **Mechanism 1:** in order to be continuously ejected in the near-wall region, a particle must
 1. meet the “right” streaks (the low-speed ones)
 2. at the “right” time (when the streaks are strong enough, namely near the separation region)
 - **Mechanism 2:** in order to be re-entrained far away from the wall (long-term resuspension), a particle must
 1. meet the “right” vortices (the rolled-up, rib-like vortices)
 2. at the “right” time and place (in the low-speed regions between lifted fluid streaks)





However, most of the times inertia is not the only source of bias!

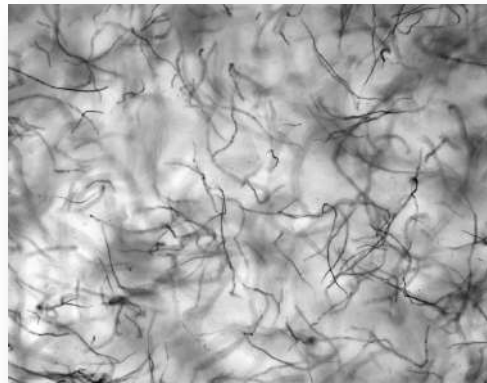
- Non-sphericity



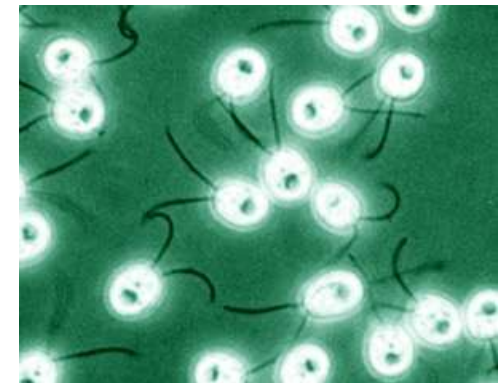
Complexity arises from

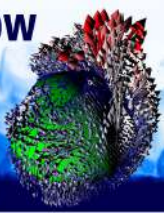
Anisotropy of turbulence
+
Anisotropy of particles

- Flexibility



- Motility





Source of bias (in this talk): Non-sphericity, flexibility & motility



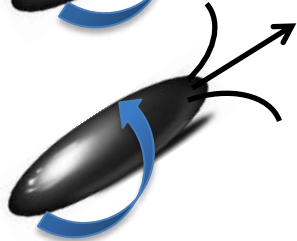
$\mathbf{x}(t), \mathbf{v}(\mathbf{x}(t), t)$



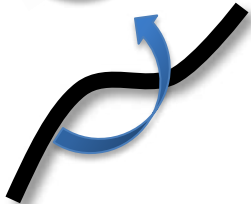
$\mathbf{x}(t), \mathbf{v}(\mathbf{x}(t), t), \omega(\mathbf{x}(t), t)$



$\mathbf{x}(t, \lambda), \mathbf{v}(\mathbf{x}(t, \lambda), t, \lambda), \omega(\mathbf{x}(t, \lambda), t, \lambda)$

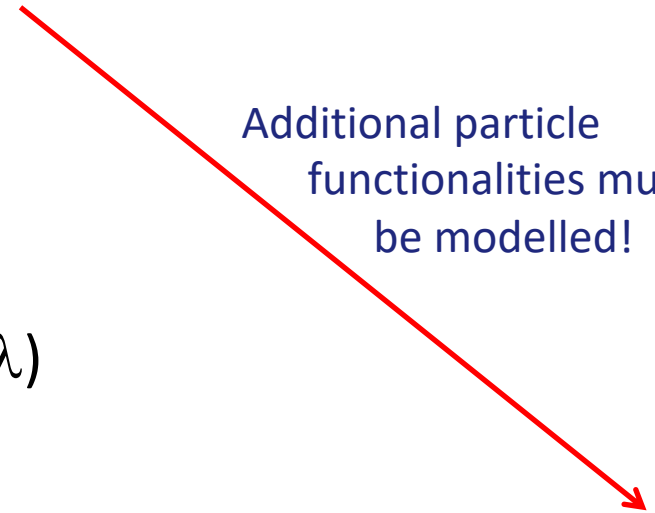


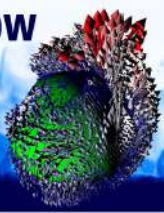
$\mathbf{x}(t, \lambda), \mathbf{v}(\mathbf{x}(t, \lambda), t, \lambda), \omega(\mathbf{x}(t, \lambda), t, \lambda), \mathbf{p}(\mathbf{x}(t, \lambda), t, \lambda)$



$\mathbf{x}(t, \lambda), \mathbf{v}(\mathbf{x}(t, \lambda), t, \lambda), \omega(\mathbf{x}(t, \lambda), t, \lambda), \mathbf{p}(\mathbf{x}(t, \lambda), t, \lambda), \psi(\mathbf{x}(t, \lambda), t, \lambda)$

Additional particle
functionalities must
be modelled!

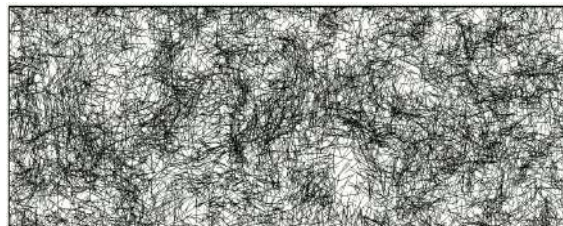
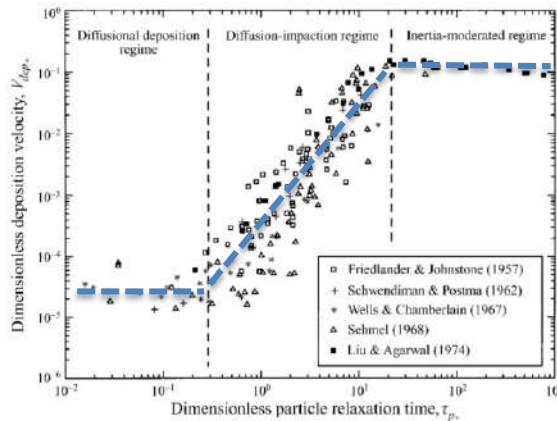
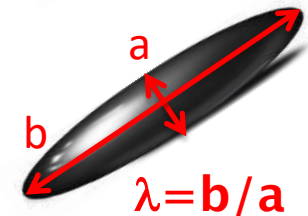
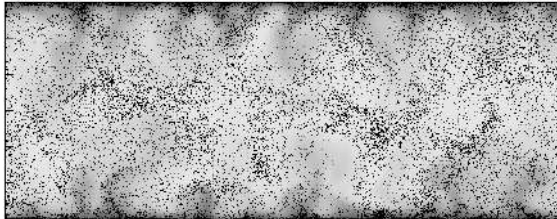




DNS of particle-laden turbulent channel flow

NS
$$\frac{\partial \mathbf{u}}{\partial t} = -(\mathbf{u} \cdot \nabla) \mathbf{u} + \frac{1}{Re_\tau} \nabla^2 \mathbf{u} - \nabla p + \mathbf{F}$$

LPT
$$\frac{d\mathbf{v}_{p_i}}{dt} = \sum F_{p_i}, \quad \frac{d\mathbf{x}_{p_i}}{dt} = \mathbf{v}_{p_i}, \quad i = 1, \dots, N$$



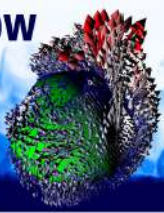
One-way coupling DATABASE:

**Spherical
particles**

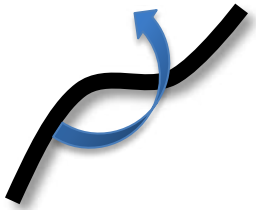
Re_τ	150, 300
St	1, 4, 5, 20, 25, 100, 125

Flexible fibers

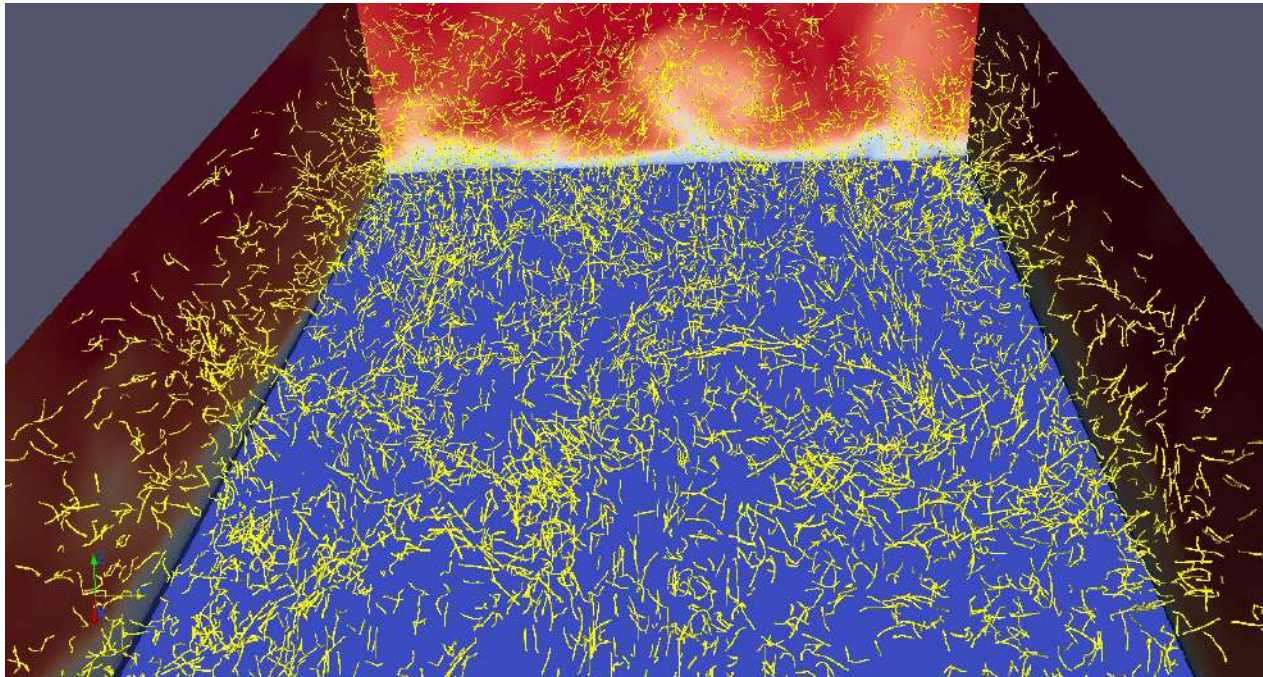
Re_τ	150, 300
St_r	1, 5, 30
λ_r	2, 5

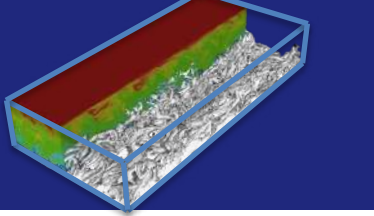


Sources of bias: Non-sphericity & Flexibility



$$\mathbf{x}(t,\lambda), \mathbf{v}(\mathbf{x}(t,\lambda),t,\lambda), \boldsymbol{\omega}(\mathbf{x}(t,\lambda),t,\lambda), \mathbf{p}(\mathbf{x}(t,\lambda),t,\lambda), \psi(\mathbf{x}(t,\lambda),t,\lambda)$$





Modelling flexibility: How to “mimic” a flexible fiber?

Bead model: flexible fiber = chain of segments/spheres connected by ball-and-socket joints (Delmotte et al '15; Andric et al '13; Slowicka et al '13; Derksen '10; Lindstrom & Uesaka '07)

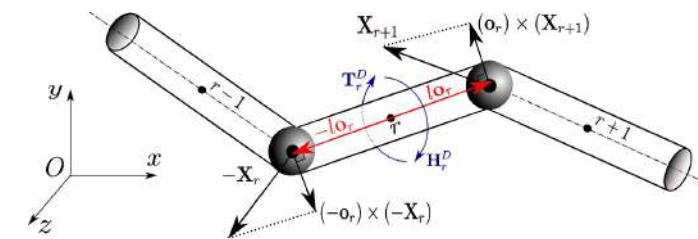
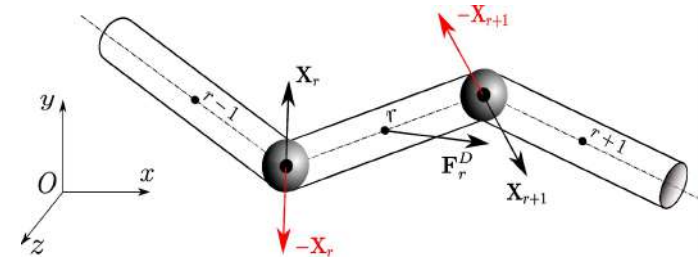
- Solve for Euler's 1st and 2nd law for each segment:

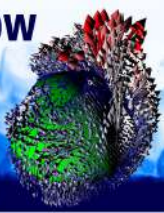
$$m_p \frac{d\mathbf{v}_r}{dt} = \mathbf{F}_r^D + (\mathbf{X}_{r+1} - \mathbf{X}_r)$$

$$\frac{d(\bar{\mathbf{J}}_r \boldsymbol{\omega}_r)}{dt} = \mathbf{T}_r^D + \mathbf{H}_r^D + l \mathbf{o}_r \times (\mathbf{X}_{r+1} + \mathbf{X}_r)$$

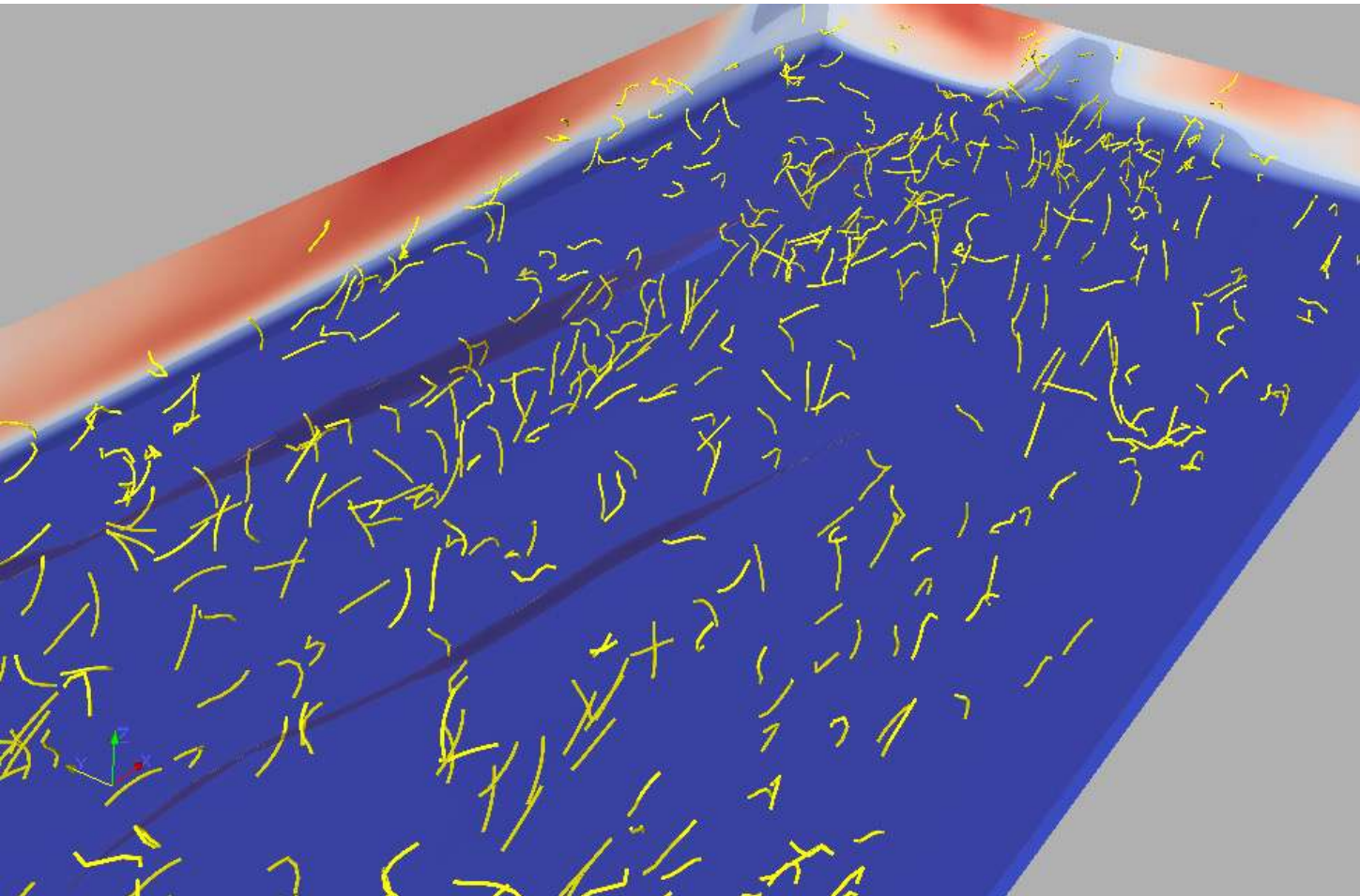
- Impose connectivity constraints between segments:

$$\begin{cases} \frac{\partial \Psi_r}{\partial t} = \mathbf{v}_{r+1} - \mathbf{v}_r + \lambda a (\boldsymbol{\omega}_r \times \mathbf{o}_r + \boldsymbol{\omega}_{r+1} \times \mathbf{o}_{r+1}) = \mathbf{0} \\ \Psi_r|_{t=0} = 0 \end{cases} \quad \Psi_r = \mathbf{p}_r + l \mathbf{o}_r - (\mathbf{p}_{r+1} - l \mathbf{o}_{r+1}) = \mathbf{0}$$





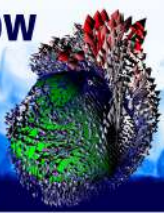
Near-wall accumulation of flexible fibers in turbulent channel flow



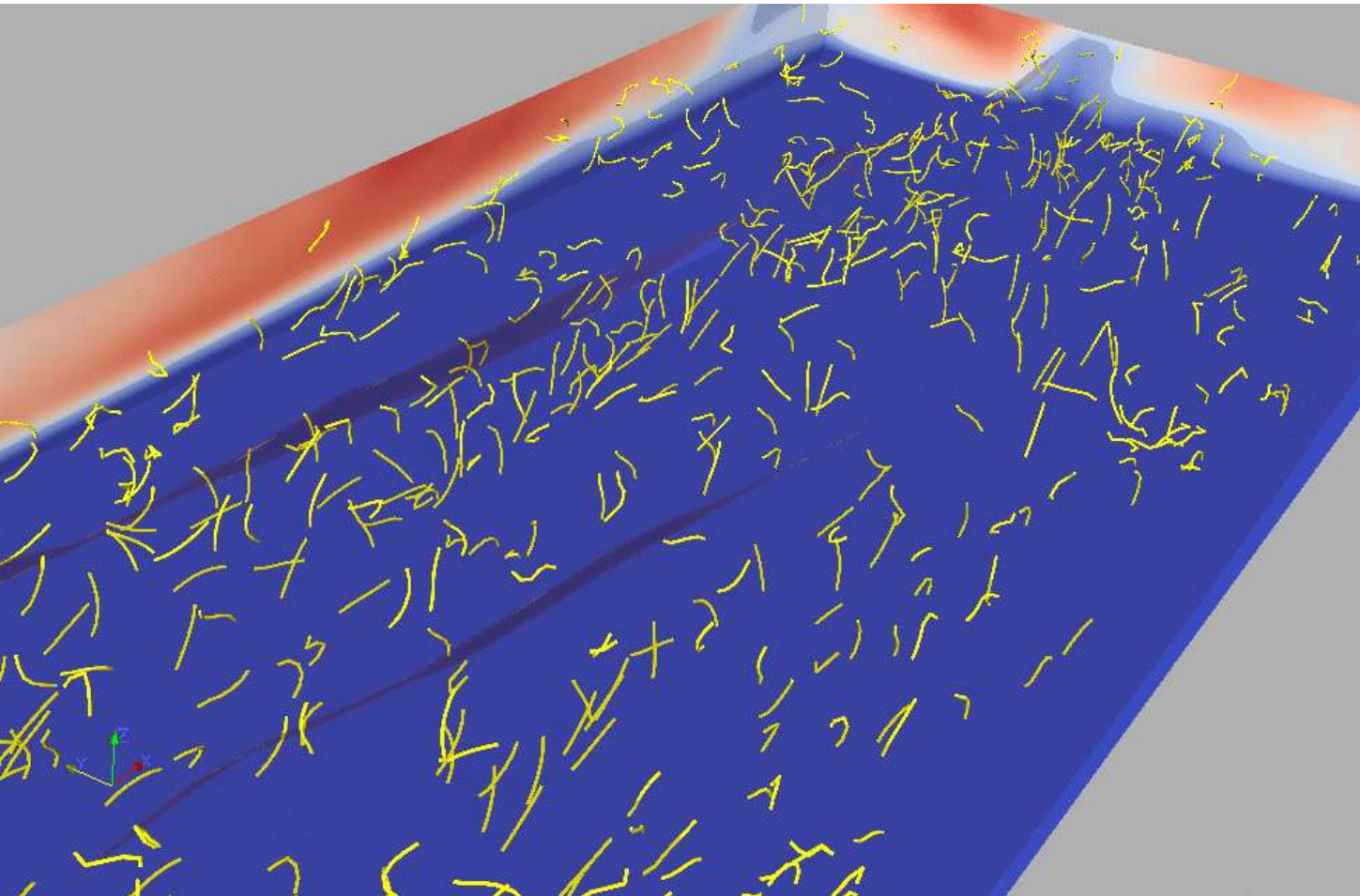
Dilute suspension of small flexible fibers in turbulent channel flow

- Shear Reynolds number: $Re_\tau=150$
- Segment Stokes number: $St_r=5$
- Segment aspect ratio: $\lambda_r=5$
- Number of segments: 7
- Number of fibers: 200,000





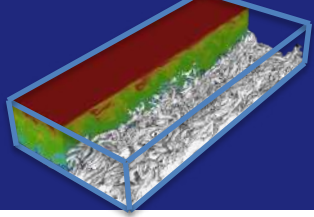
Near-wall accumulation of flexible fibers in turbulent channel flow



Dilute suspension of small flexible fibers in turbulent channel flow

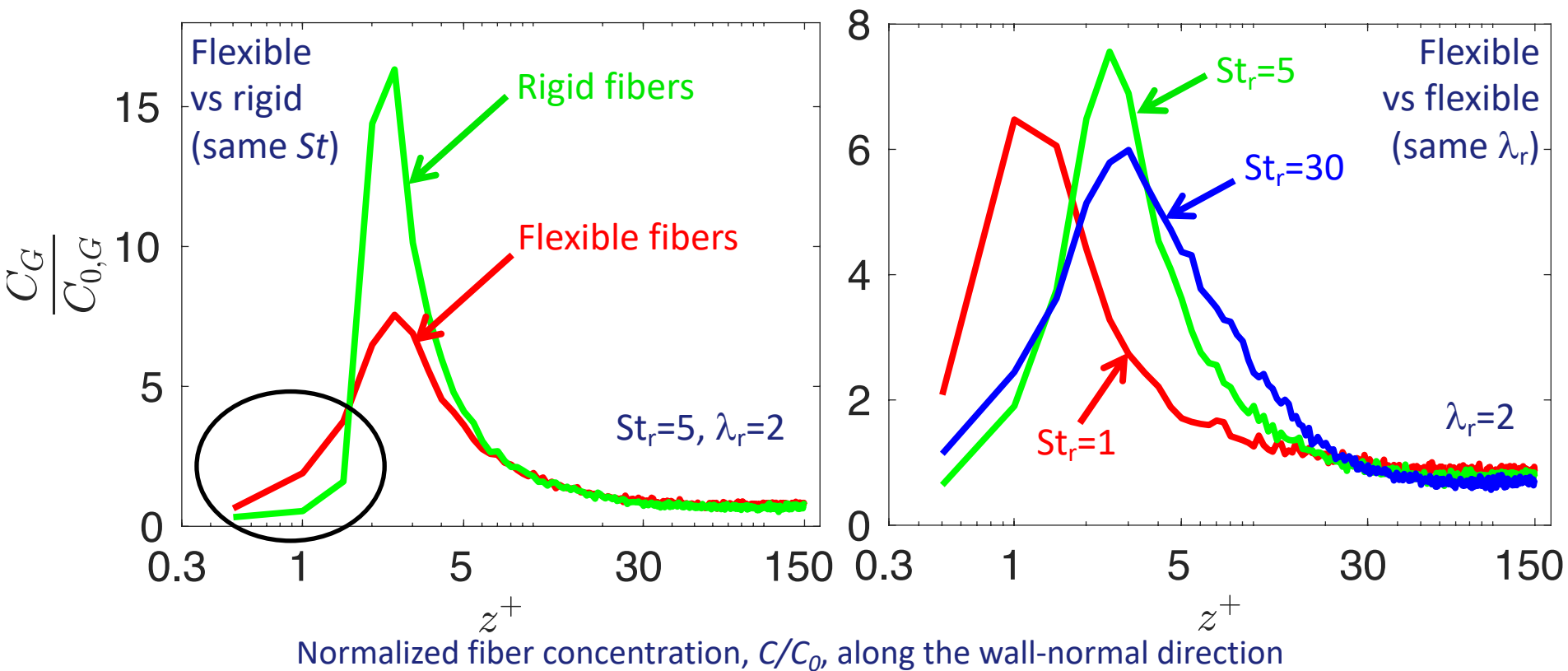
- Shear Reynolds number: $Re_\tau=150$
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- Number of fibers: 200,000





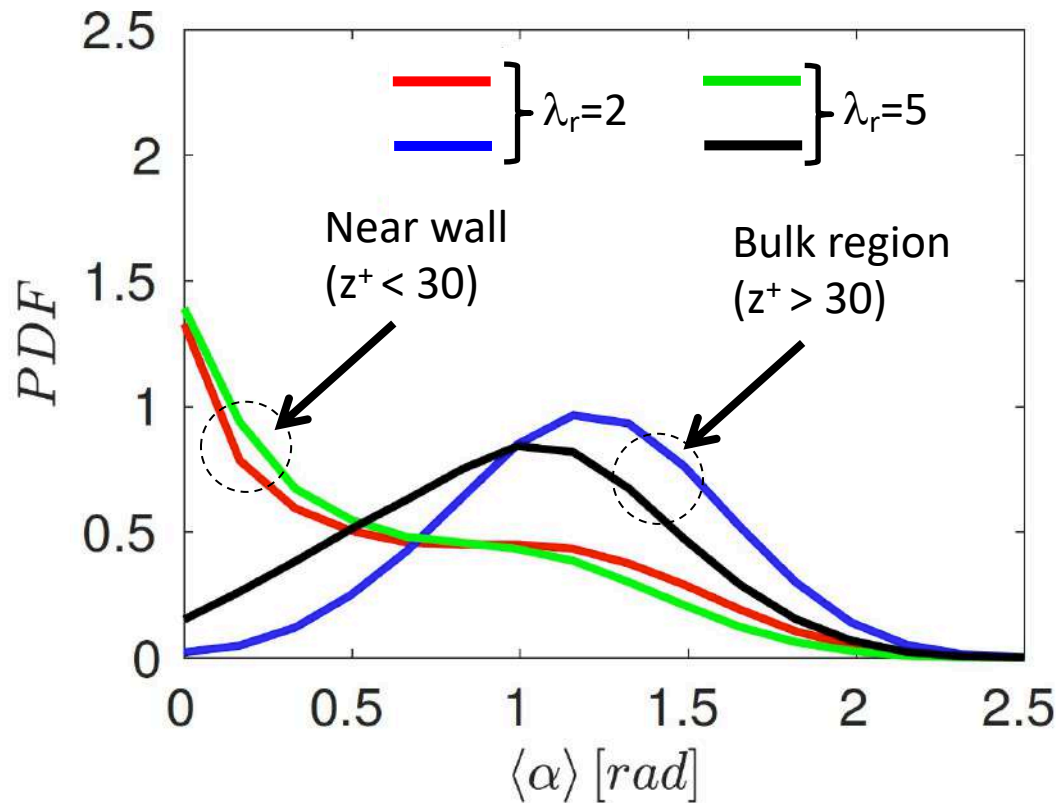
Near-wall accumulation of flexible fibers in turbulent channel flow

Effect of flexibility on near-wall accumulation

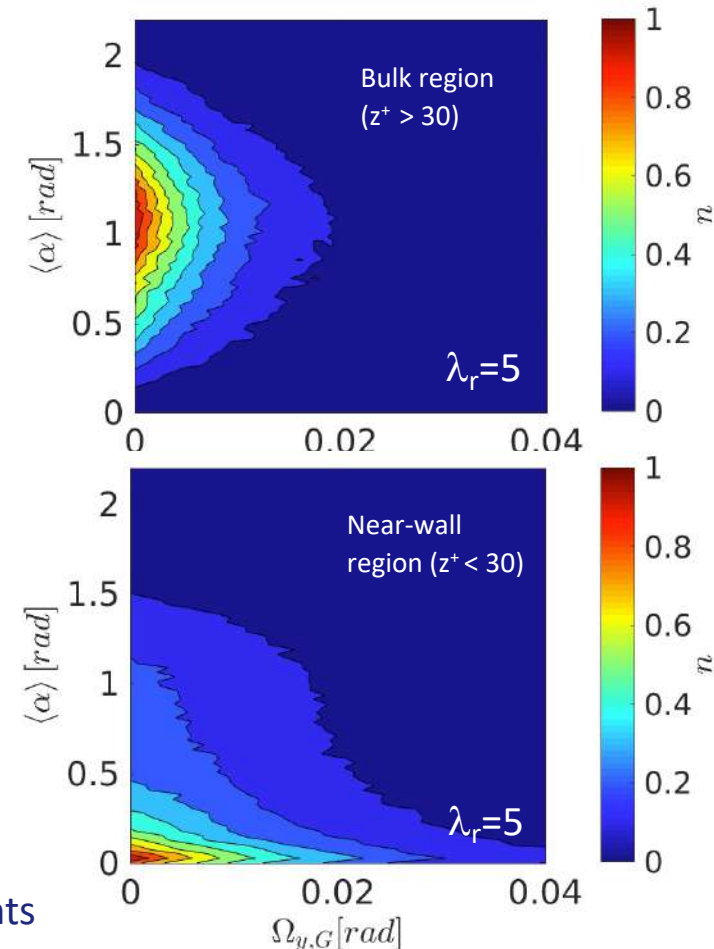


Deformation of flexible fibers in turbulent channel flow

Effect of flexibility on bending (for $St_r=30$)

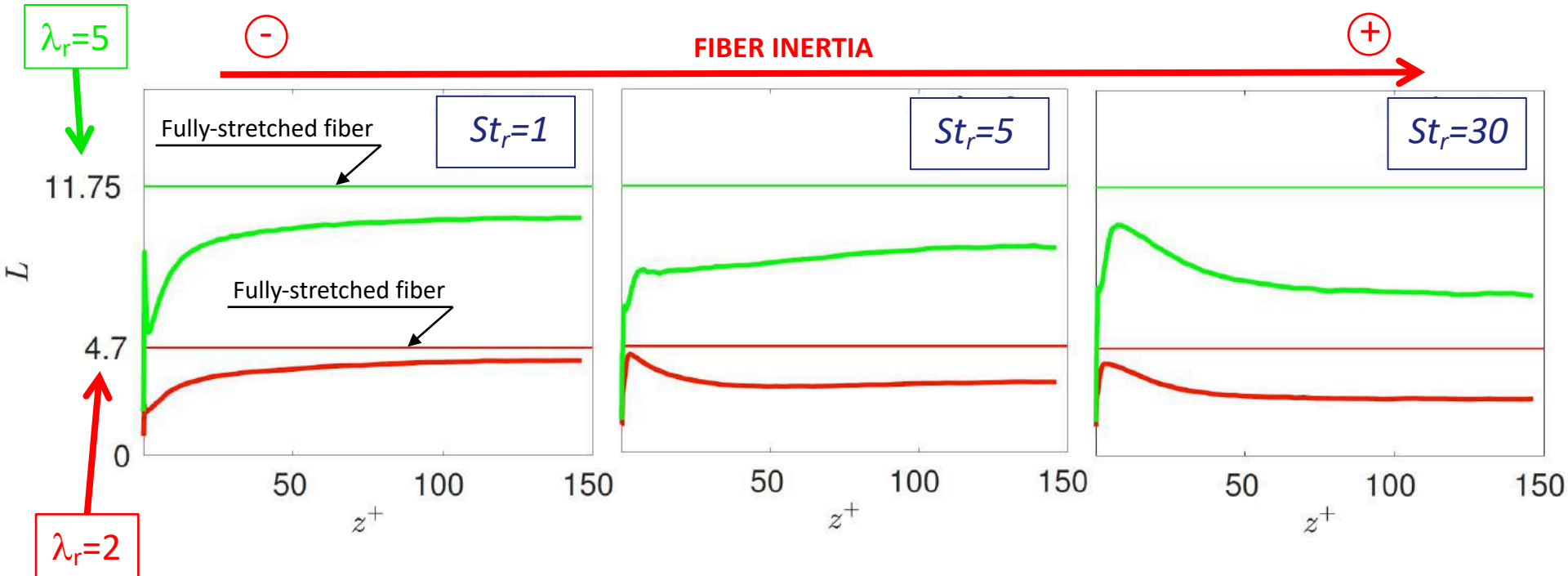


PDF of relative orientation between neighboring fiber elements



Deformation of flexible fibers in turbulent channel flow

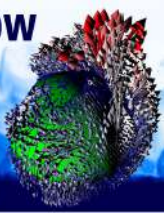
Fiber “end-to-end” distance along the wall-normal direction



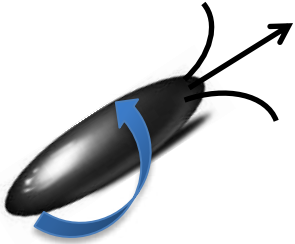
Fiber bending dynamics change with fiber inertia:

Flexible fibers with low inertia are more stretched by turbulence in the bulk flow region
(higher bending near the wall)

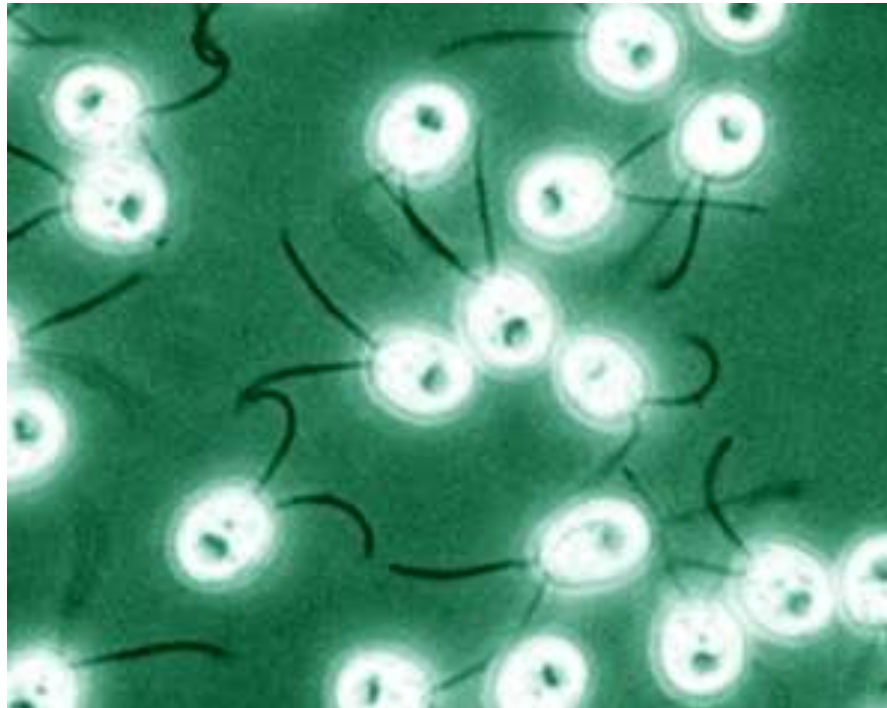
Flexible fiber with large inertia are more stretched by turbulence in the near-wall region



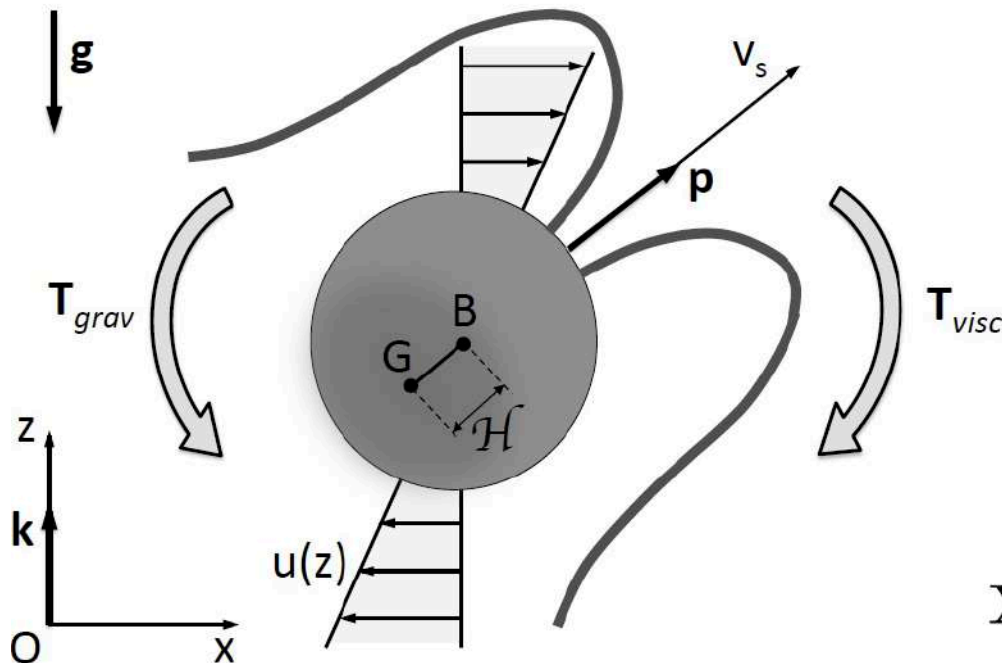
Source of bias: Motility



$$\mathbf{x}(t, \lambda), \mathbf{v}(\mathbf{x}(t, \lambda), t, \lambda), \omega(\mathbf{x}(t, \lambda), t, \lambda), \mathbf{p}(\mathbf{x}(t, \lambda), t, \lambda)$$



Effect of particle motility on preferential concentration



Swimming provides a way for micro-organisms to escape fluid streamlines (Kessler, *Hydrodynamic focusing of motile algal cells*, Nature, 1985)

Gyrotaxis: any directed locomotion resulting from the combination of gravitational and viscous torques in a flow

Assumptions :

- dilute suspension of neutrally-buoyant micro-organisms
- Sub-Kolmogorov size
- Negligible inertia
- Swimming at constant \mathbf{v}_s aligned with \mathbf{p}

$$\dot{\mathbf{X}} = \mathbf{u}(\mathbf{X}, t) + v_s \mathbf{p}$$

$$\dot{\mathbf{p}} = \underbrace{\frac{1}{2B} [\mathbf{k} - (\mathbf{k} \cdot \mathbf{p}) \mathbf{p}]}_{\text{Re-orientation term due to gravitational torque}} + \underbrace{\frac{1}{2} \boldsymbol{\omega} \times \mathbf{p}}_{\text{Vorticity term}}$$

Effect of particle motility on preferential concentration

Two controlling parameters:

$$V_s \simeq 10 - 1000 \mu m/s \longrightarrow \Phi = v_s / u_\tau \quad \text{Swimming number}$$

$$B \simeq 0.1 - 10 s \longrightarrow \Psi = \frac{1}{2B} \frac{\nu}{u_\tau^2} \quad \text{Stability number}$$

Values considered in our study:

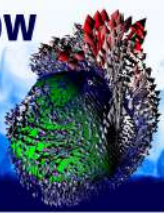


$$\Phi = 0.048 \quad \text{Dimensionless swimming speed}$$

$$\Psi_L = 0.0113 \quad \text{Low gravitaxis (slow re-orientation)} \quad \blacktriangleright \Psi_L \cdot \tau_{K,max}^+ \sim \mathcal{O}(10^{-1})$$

$$\Psi_I = 0.113 \quad \text{Intermediate gravitaxis} \quad \blacktriangleright \Psi_I \cdot \tau_{K,max}^+ \sim \mathcal{O}(1)$$

$$\Psi_H = 1.13 \quad \text{High gravitaxis (fast re-orientation)} \quad \blacktriangleright \Psi_H \cdot \tau_{K,max}^+ \sim \mathcal{O}(10)$$



Physical problem and flow configuration

Flow solver:

$$\frac{\partial u_i}{\partial x_i} = 0$$

$$\rho \left(\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right) = - \frac{\partial P}{\partial x_i} + \mu \frac{\partial^2 u_i}{\partial x_j^2}$$

- 3D time-dependent turbulent water flow
- Shear Reynolds number:

$Re_\tau = 171, 510, 1020$

- Channel size:

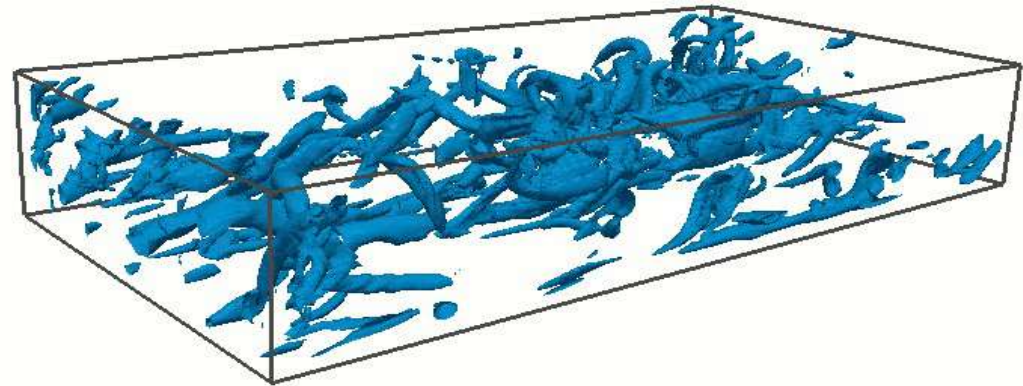
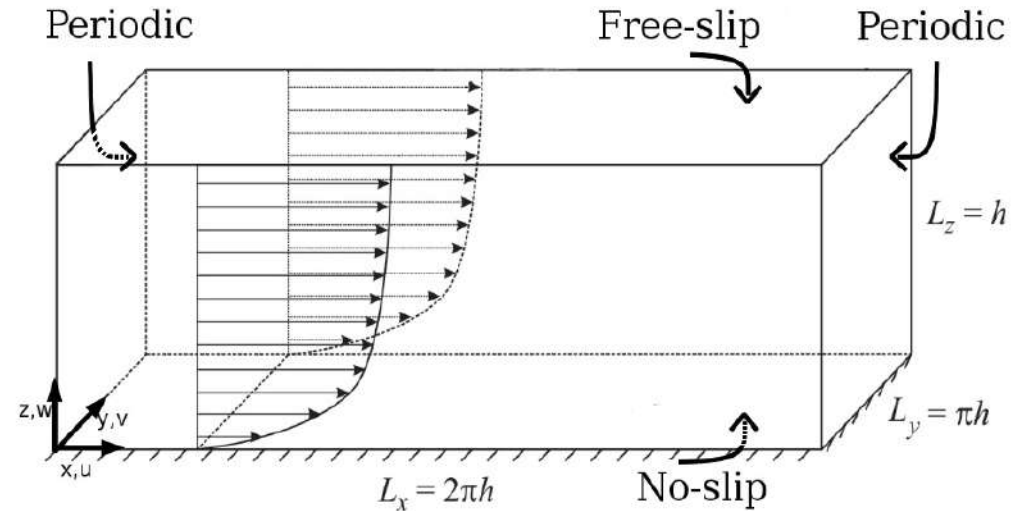
$$L_x \times L_y \times L_z = 2\pi h \times \pi h \times h$$

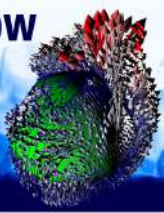
- Pseudo-spectral DNS

- Time integration:

Adams-Bashforth (convective terms)

Crank-Nicolson (viscous terms)

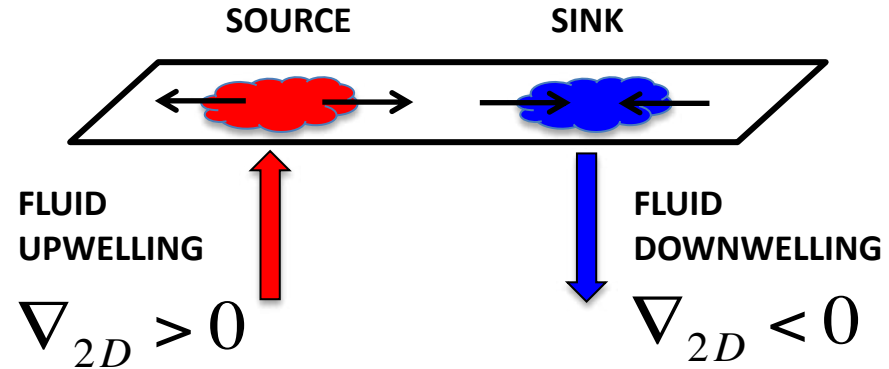




Flow topology at the free surface

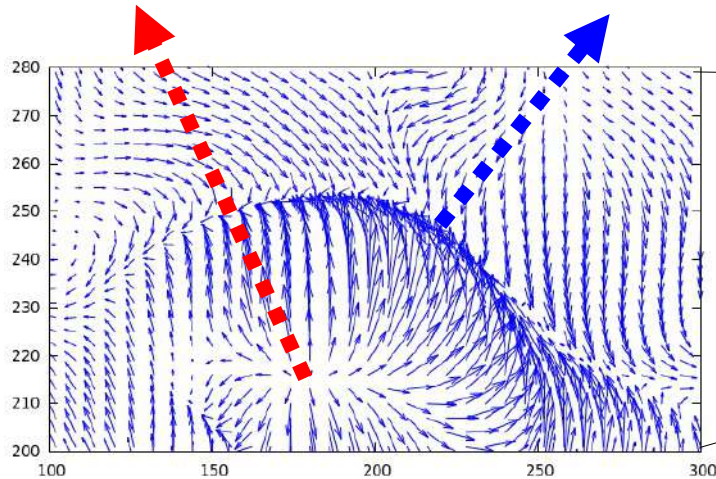
Surface divergence

$$\nabla_{2D} = \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = -\frac{\partial w}{\partial z}$$

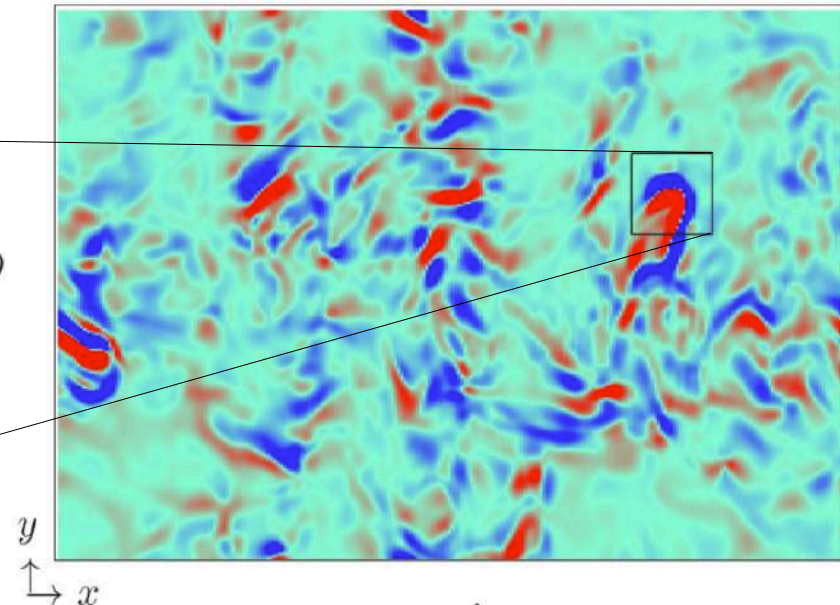


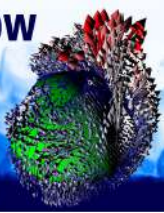
Velocity
source

Velocity
sink



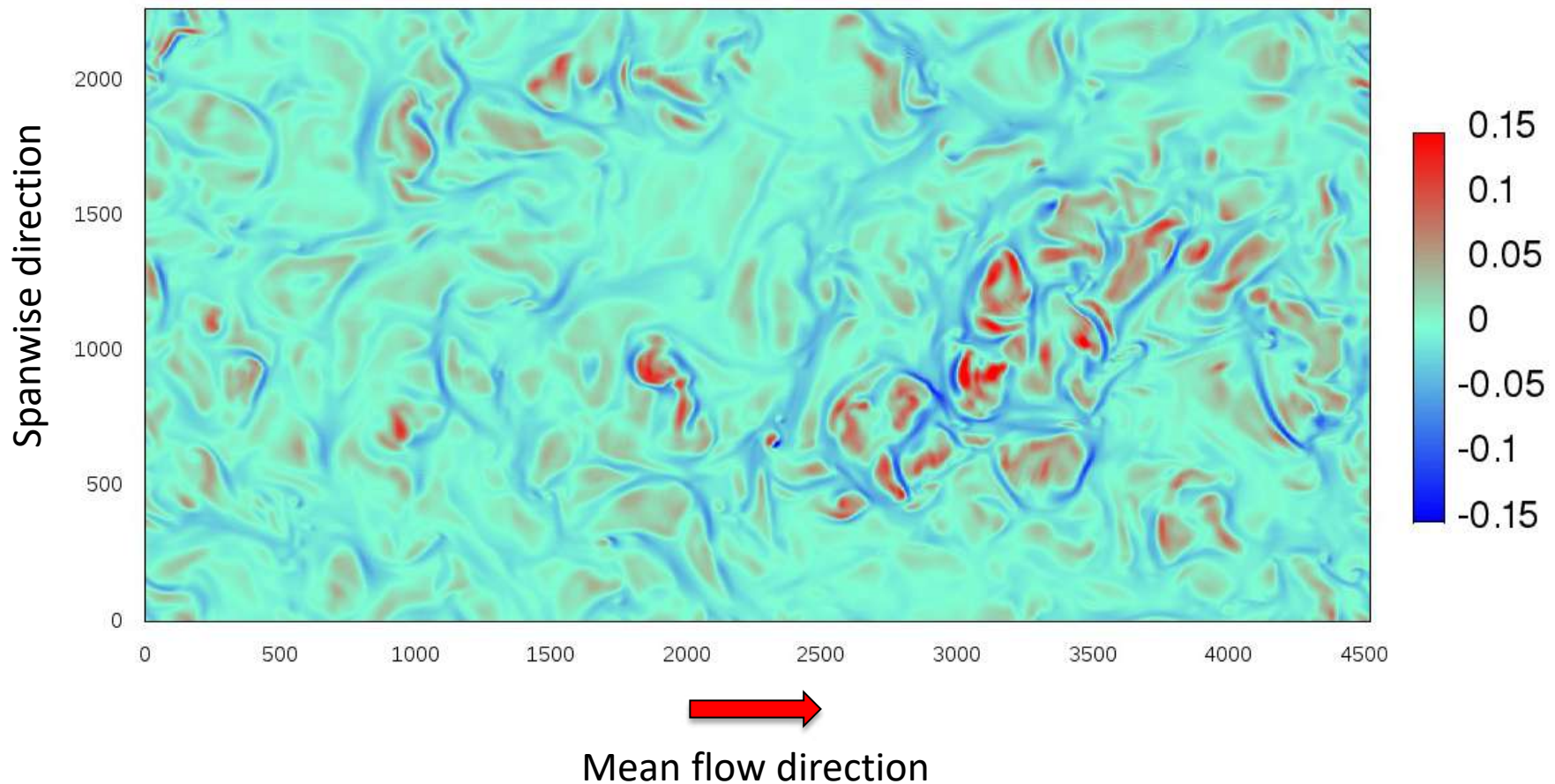
∇_{2D}

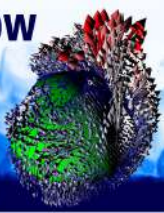




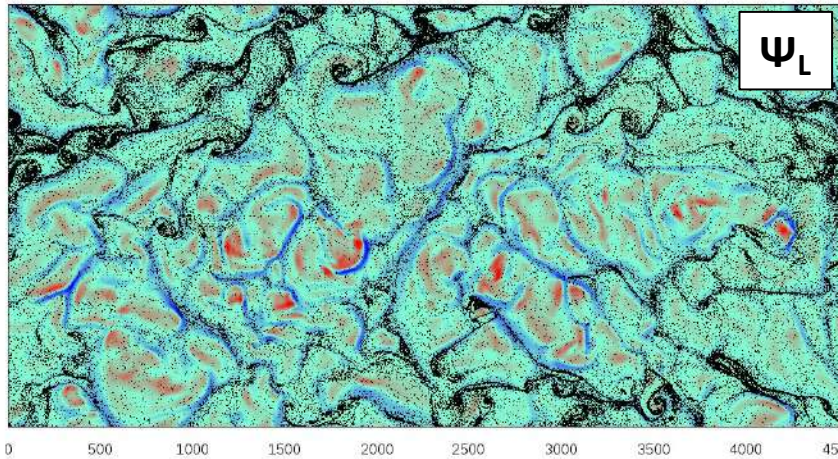
Swimmer clustering at the free surface

Top view of swimmers' surfacing

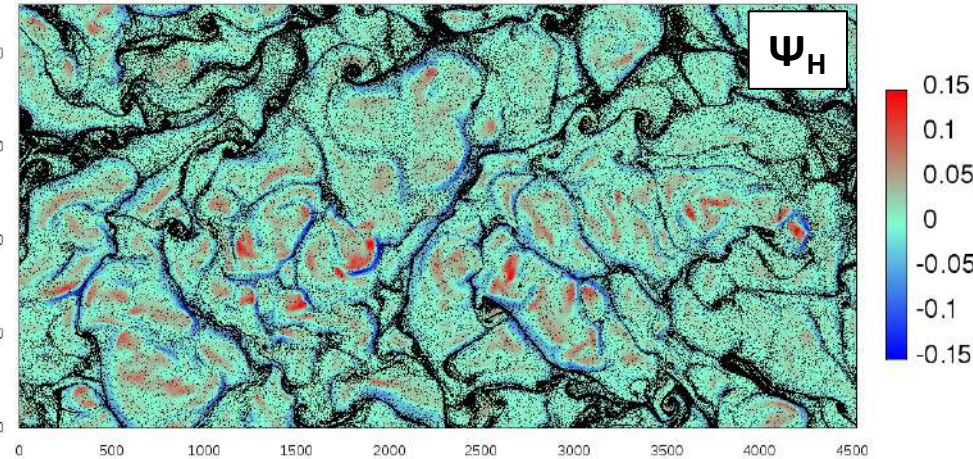




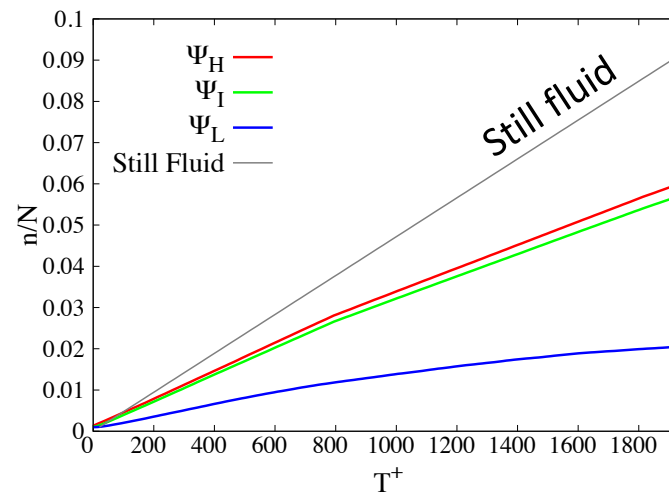
Swimmer clustering at the free surface



Slow to re-orient



Fast to re-orient



Ψ_H Fast

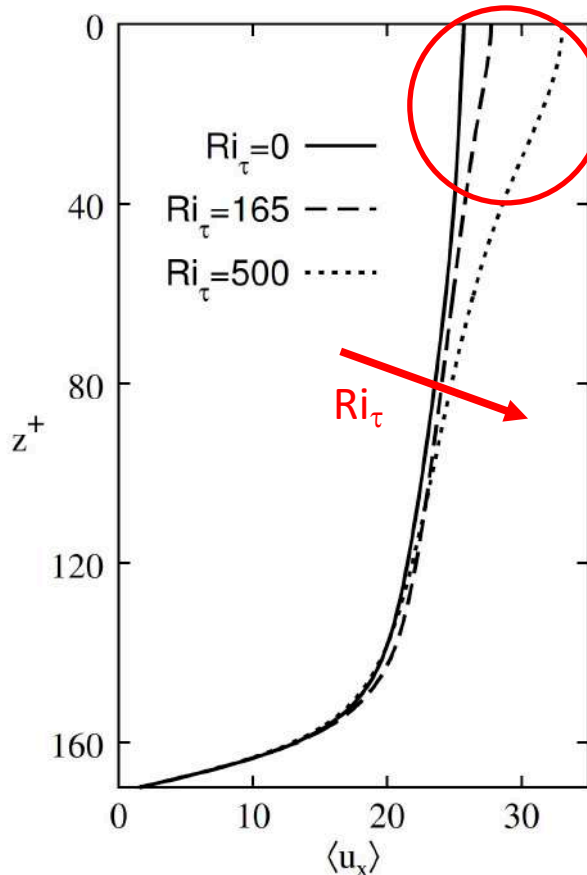
Ψ_L Slow

Swimmers that have
reached the surface: 600k

Swimmer dynamics in thermally-stratified turbulence

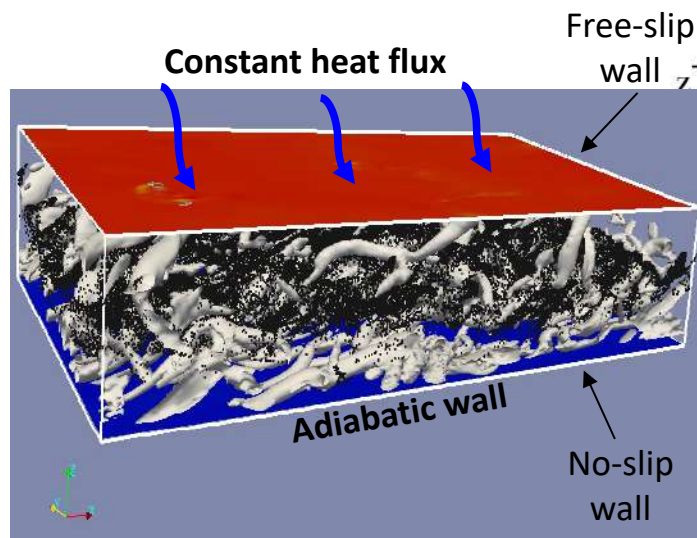
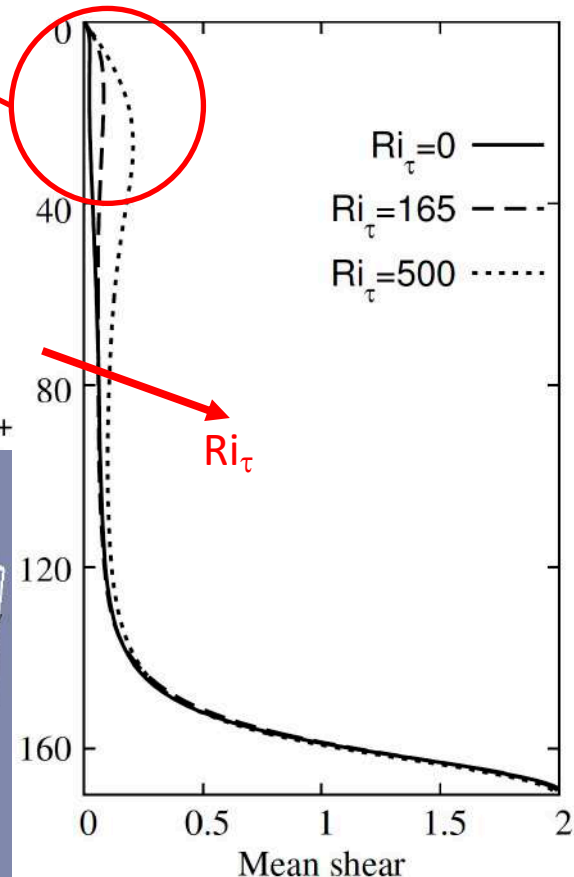
Lovecchio et al Adv. Wat. Res (2014)

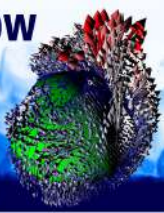
Mean streamwise velocity



“Thermocline”:
potential barrier
due to density
distribution

Mean shear

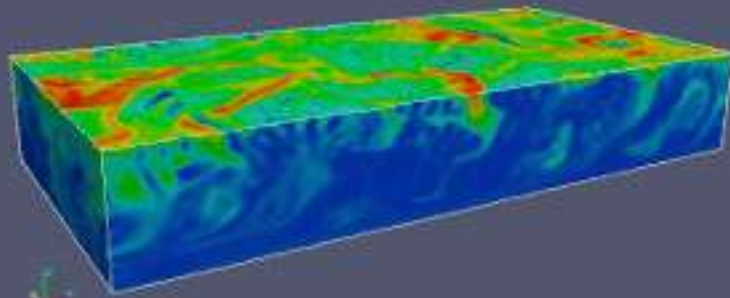




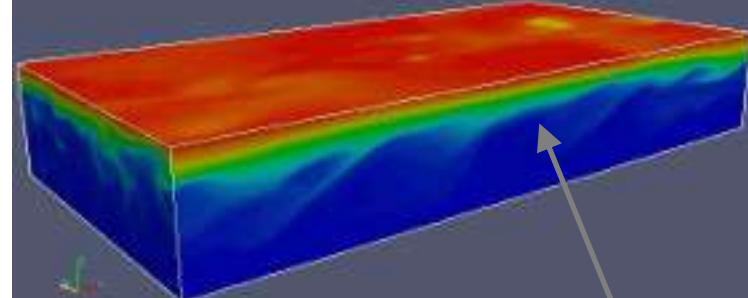
Stably-stratified turbulent channel

Temperature field

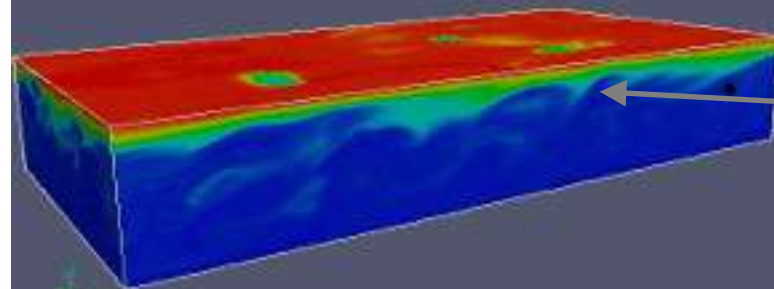
$Ri_\tau=0$



$Ri_\tau=165$



$Ri_\tau=500$



Thermocline
(barrier)

All sim. @
Re=171 &
Pr=5

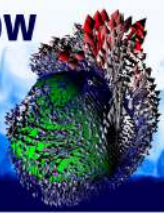
$$\nabla \cdot \mathbf{u} = 0,$$

$$\frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} = \frac{1}{Re_\tau} \nabla^2 \mathbf{u} - \nabla p + \frac{Gr}{Re_\tau^2} \theta \delta_g + \delta_p,$$

$$\frac{\partial \theta}{\partial t} + \mathbf{u} \cdot \nabla \theta = \frac{1}{Re_\tau Pr} \nabla^2 \theta - \beta_T,$$

$$Ri = \frac{Gr}{Re_\tau^2}$$

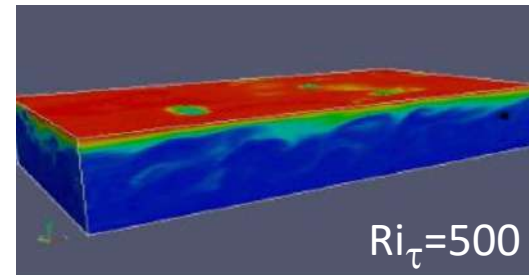
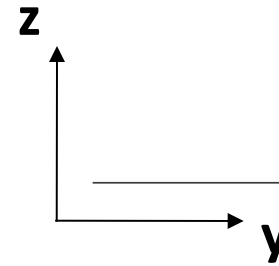
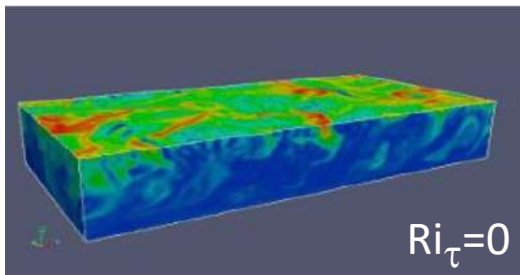
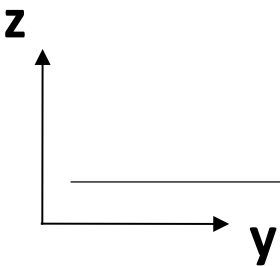
$$Gr = \frac{g \beta \frac{\partial T}{\partial z}|_{sup} (2h)^3 h}{\nu^2}$$



Vertical motion of swimmers with low stability number (Slow to realign against gravity)

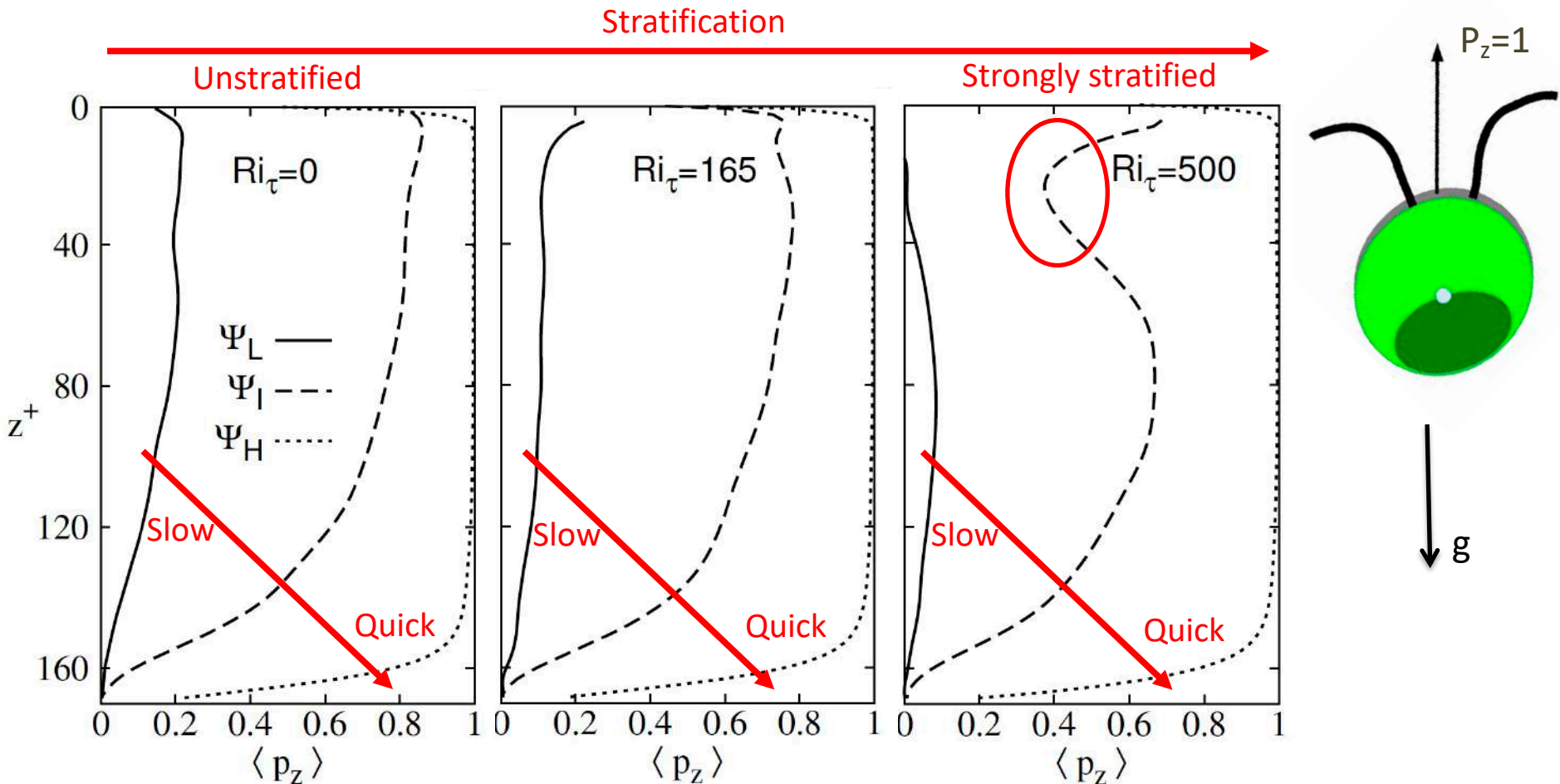
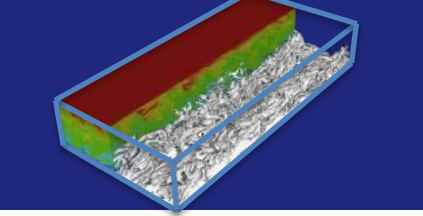
UNSTRATIFIED FLOW

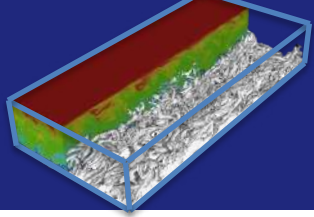
STRATIFIED FLOW



Swimmers' preferential orientation

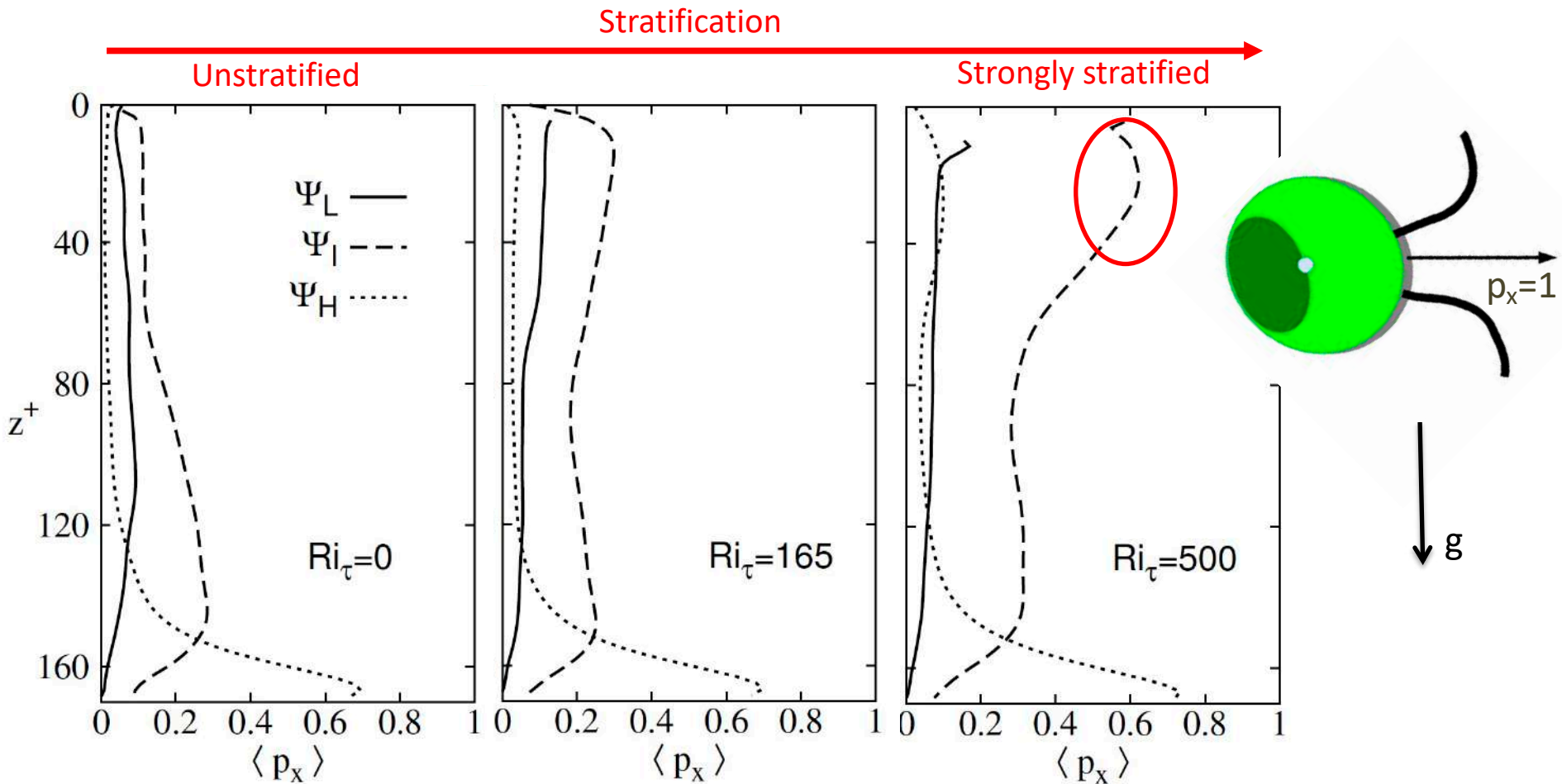
Mean orientation in vertical direction (p_z)





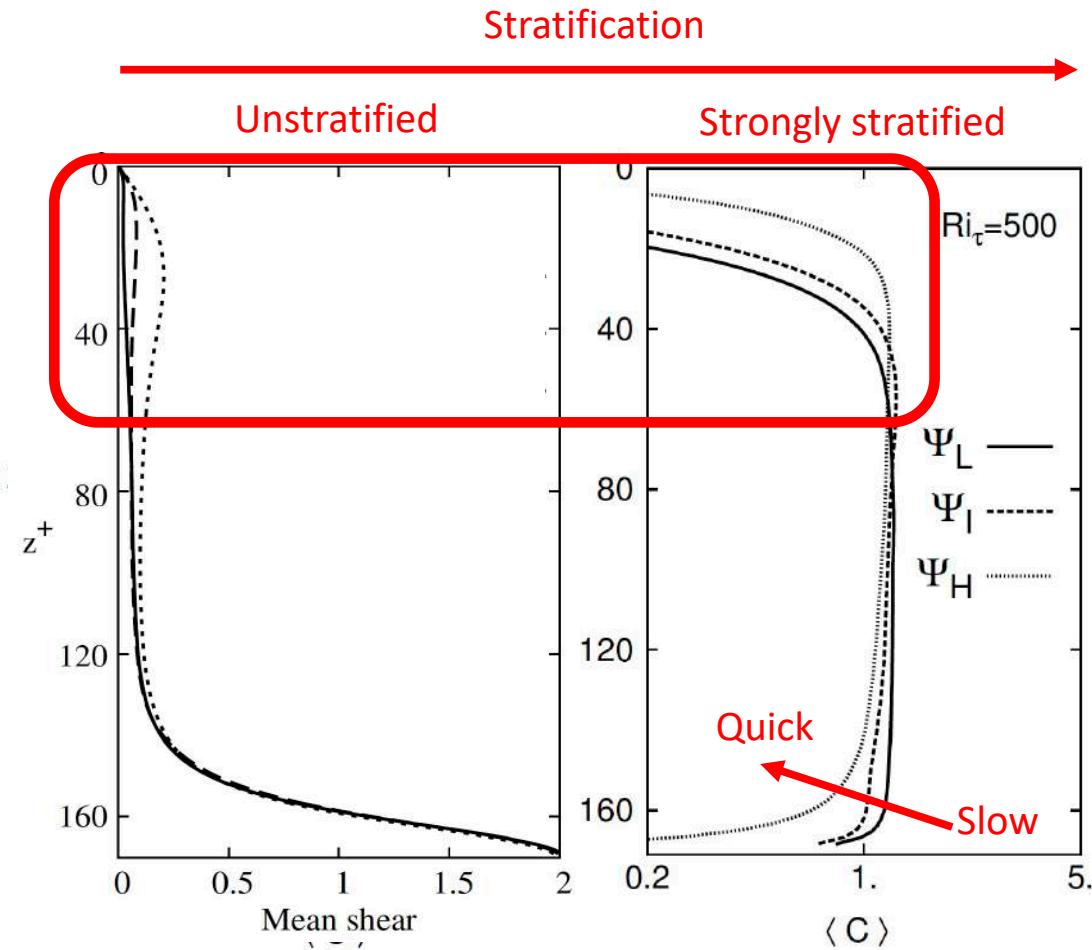
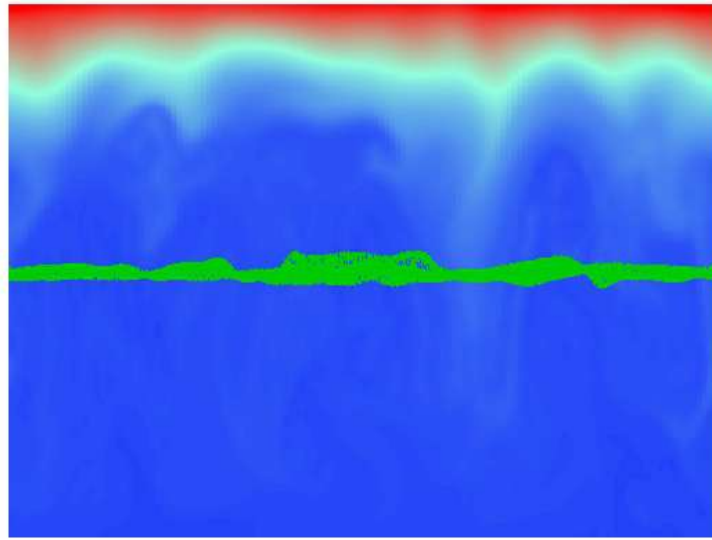
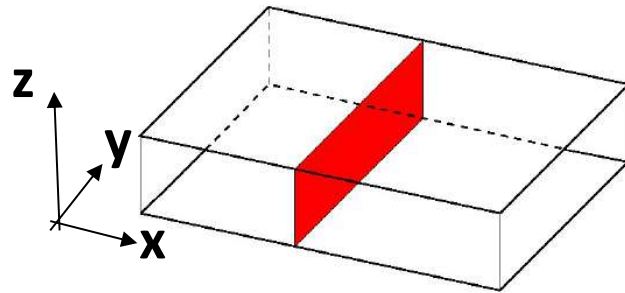
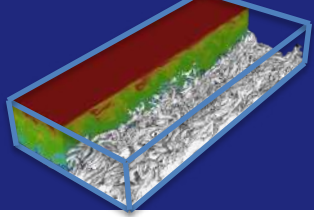
Swimmers' preferential orientation

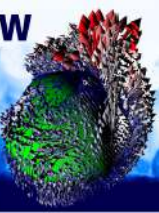
Mean orientation in horizontal direction (p_x)



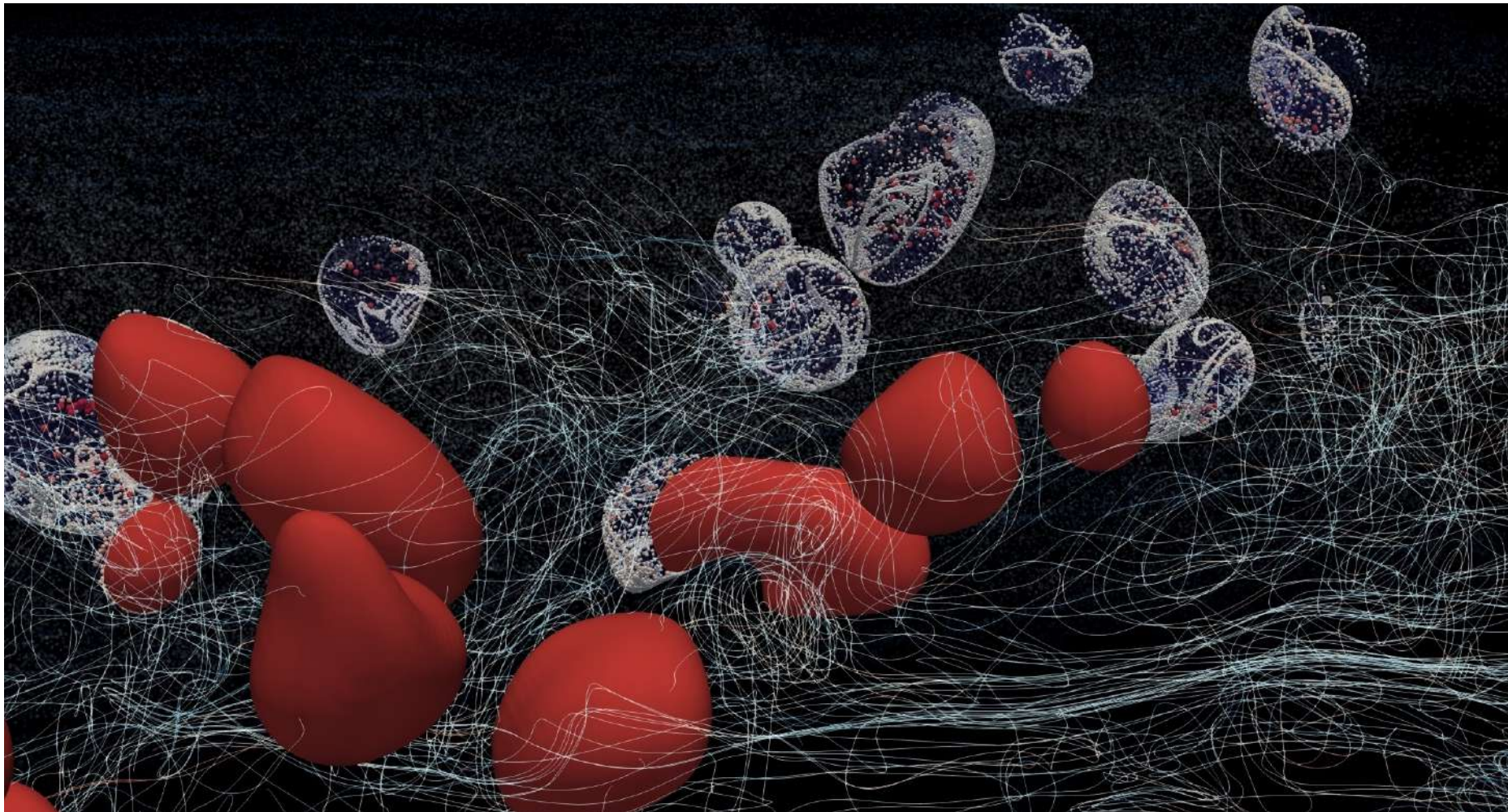
Swimmers' preferential concentration

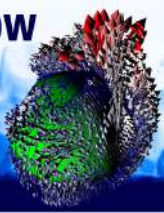
Number density in the vertical direction



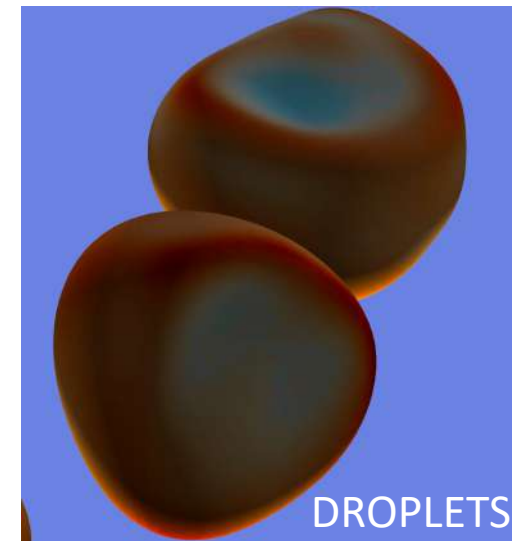
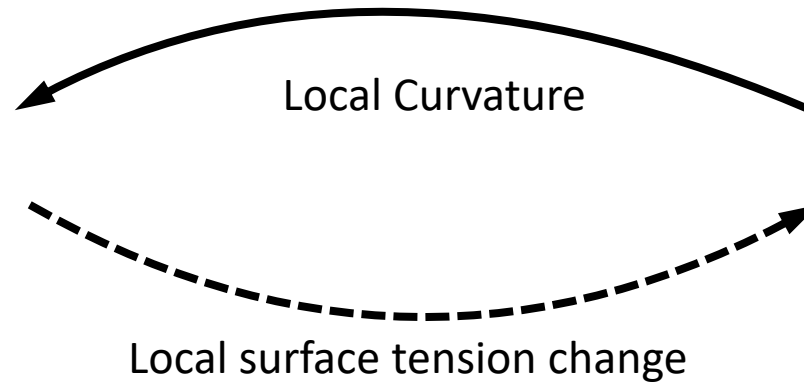
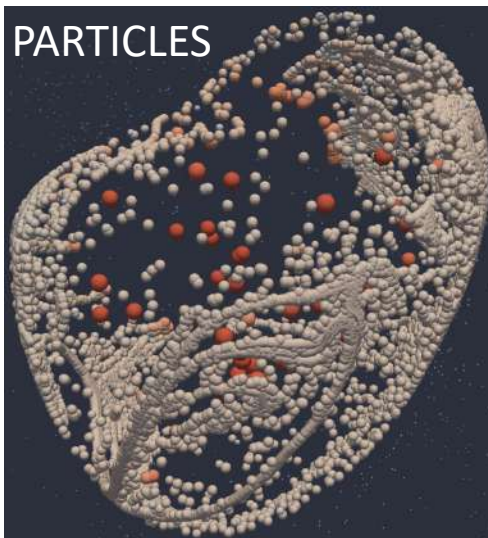
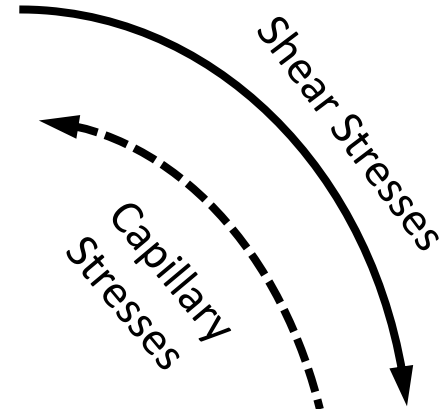
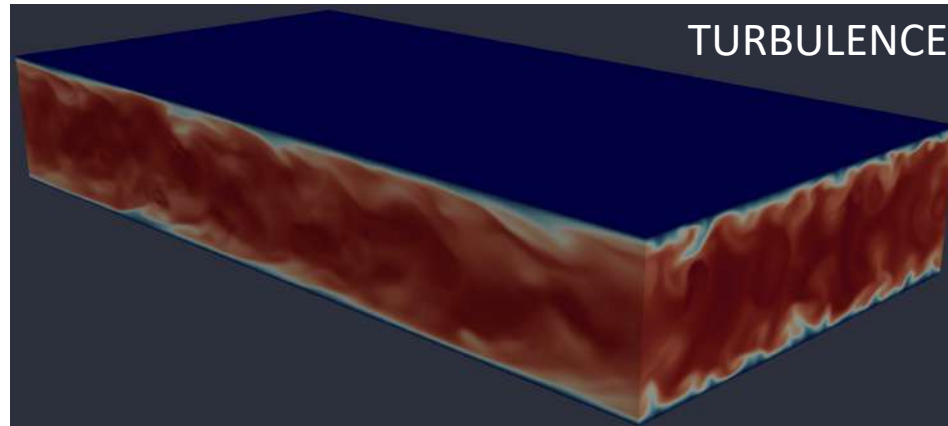
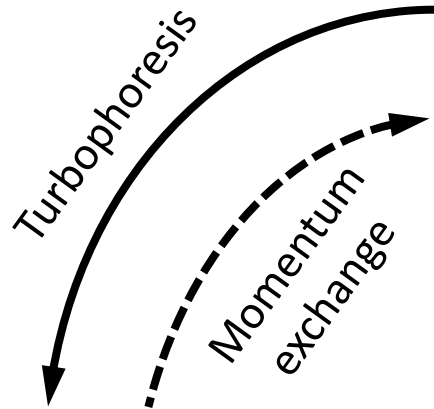
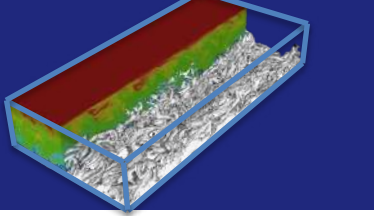


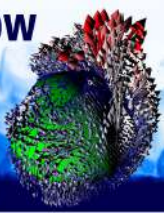
Source of bias: Fluid interface



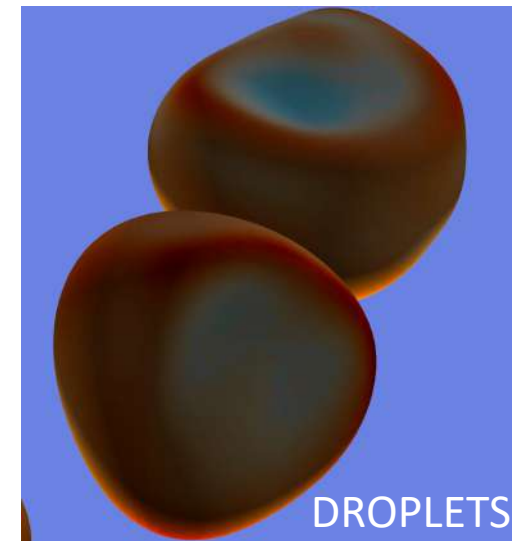
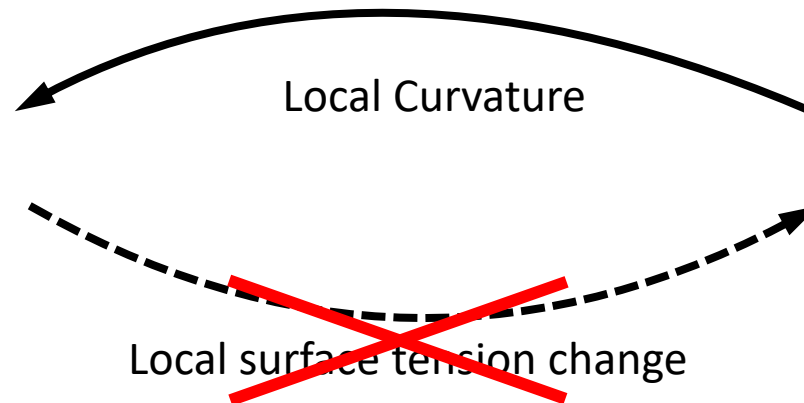
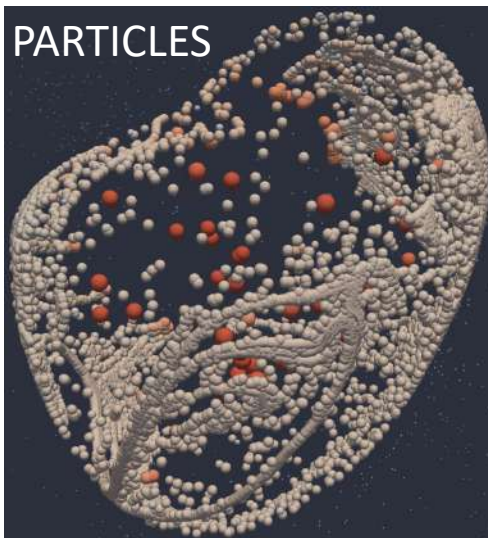
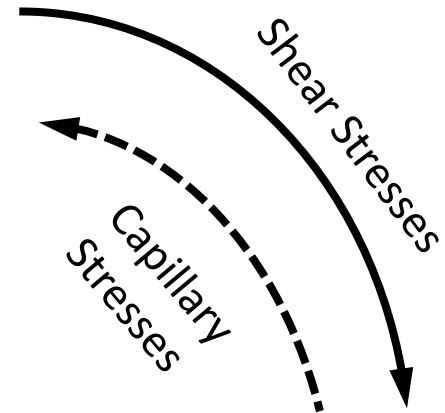
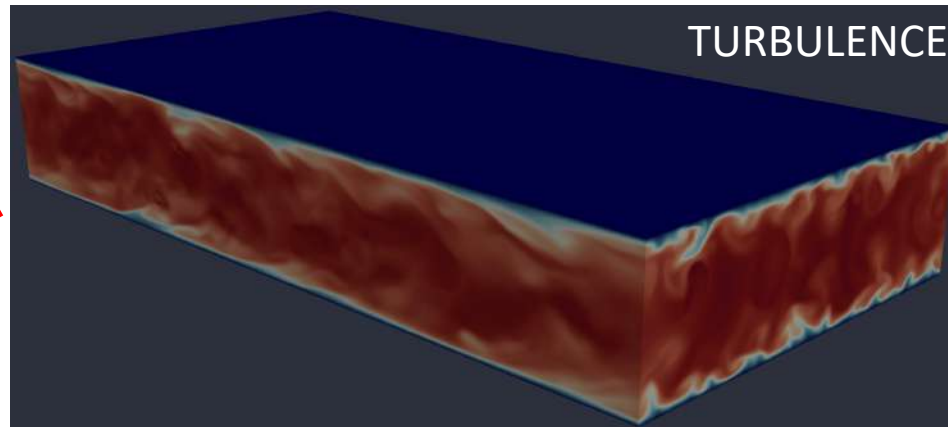
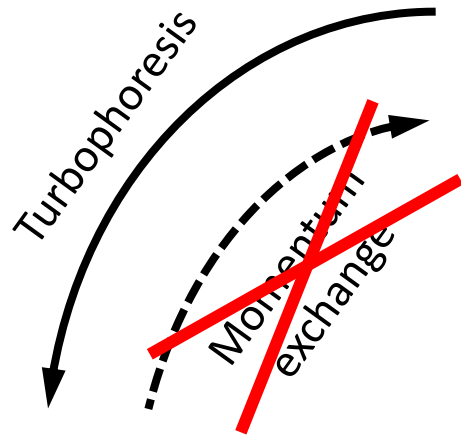
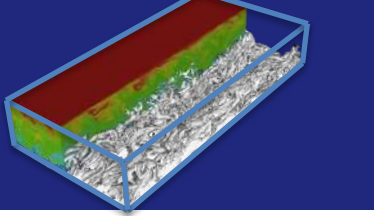


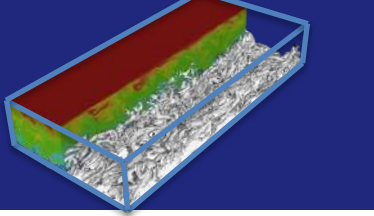
Three-phase laden flow





Three-phase laden flow





Methodology

Continuity and Navier-Stokes equation:

$$\nabla \cdot u = 0$$

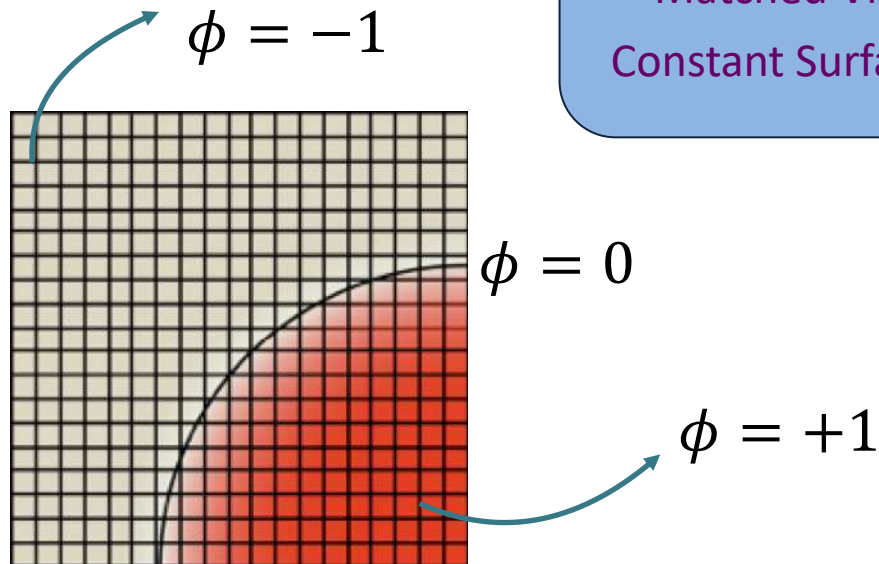
$$\frac{\partial u}{\partial t} + u \cdot \nabla u = -\nabla p + \frac{1}{Re_\tau} \nabla^2 u + \overbrace{\frac{Ch}{We} \frac{3}{\sqrt{8}} \nabla \cdot \tau_c}^{\text{Surface Tension Force}}$$

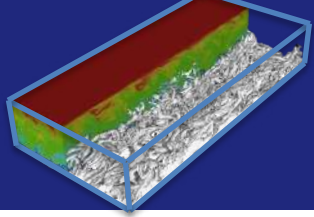
Assumptions:
Matched Density
Matched Viscosity
Constant Surface Tension

Cahn-Hilliard Equation:

$$\frac{\partial \phi}{\partial t} + u \cdot \nabla \phi = \frac{1}{Pe} \nabla^2 \mu$$

$$\mu = \phi^3 - \phi - Ch^2 \nabla^2 \phi$$





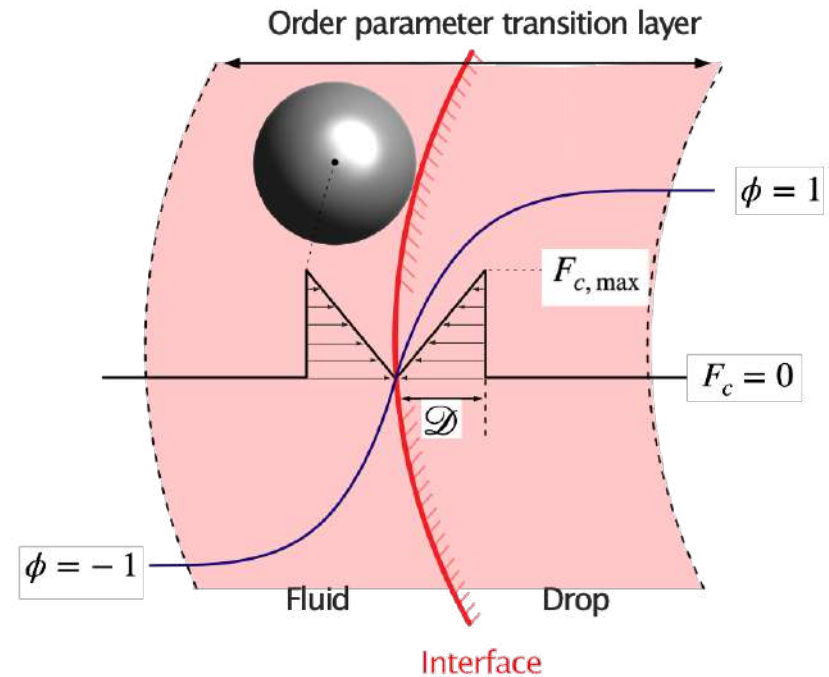
Methodology

Lagrangian Equation of Motion:

$$\frac{\partial x_p}{\partial t} = u_p$$

$$\frac{\partial u_p}{\partial t} = \underbrace{\frac{u - u_p}{St} f_D}_{\text{Drag Force}} +$$

$$\underbrace{\frac{6A}{\frac{\rho_p}{\rho_f}} \frac{Re}{We} \frac{d^+}{dp^{+3}}}_{\text{Capillary force}}$$



See: Ettelaie & Lishchuk, *Soft Matter*, 2015
Gu & Botto, *Soft Matter*, 2016

- St : Particle inertia
- d^+ : Min distance from particle center to interface
- d_p^+ : Particle diameter

$$d^+ = \frac{\sqrt{2}}{2} Ch \ln\left(\frac{1 + \phi_{pp}}{1 - \phi_{pp}}\right)$$

Simulation parameters

Flow Field:

No-slip at the walls

$$u(x, y, \pm 1) = 0$$

Phase field:

$$\frac{\partial \phi}{\partial z}(x, y, \pm 1) = 0$$

$$\frac{\partial^3 \phi}{\partial z^3}(x, y, \pm 1) = 0$$

Simulation Parameters:

Grid points = 512 x 256 x 257

Size = $4\pi h \times 2\pi h \times 2h$

Boundary conditions

Periodicity along x and y

$$u(0, y, z) = u(L_x, y, z)$$

$$u(x, 0, z) = u(x, L_y, z)$$

Periodicity along x and y

$$\phi(0, y, z) = \phi(L_x, y, z)$$

$$\phi(x, 0, z) = \phi(x, L_y, z)$$

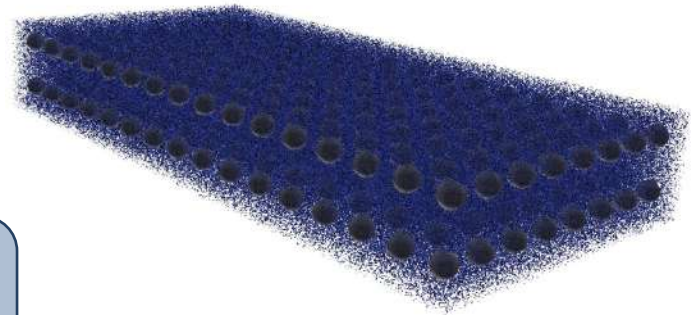
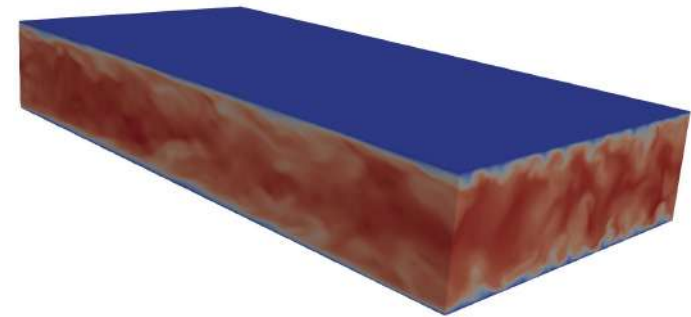
$$Re_\tau = 150$$

$$We = 0.75, 1.5$$

$$St = 0.1, \dots, 0.8$$

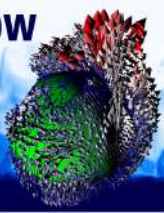
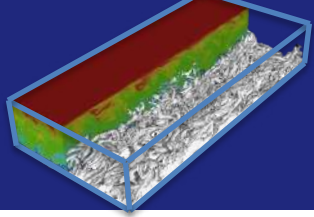
Initial Condition

Fully developed turbulence

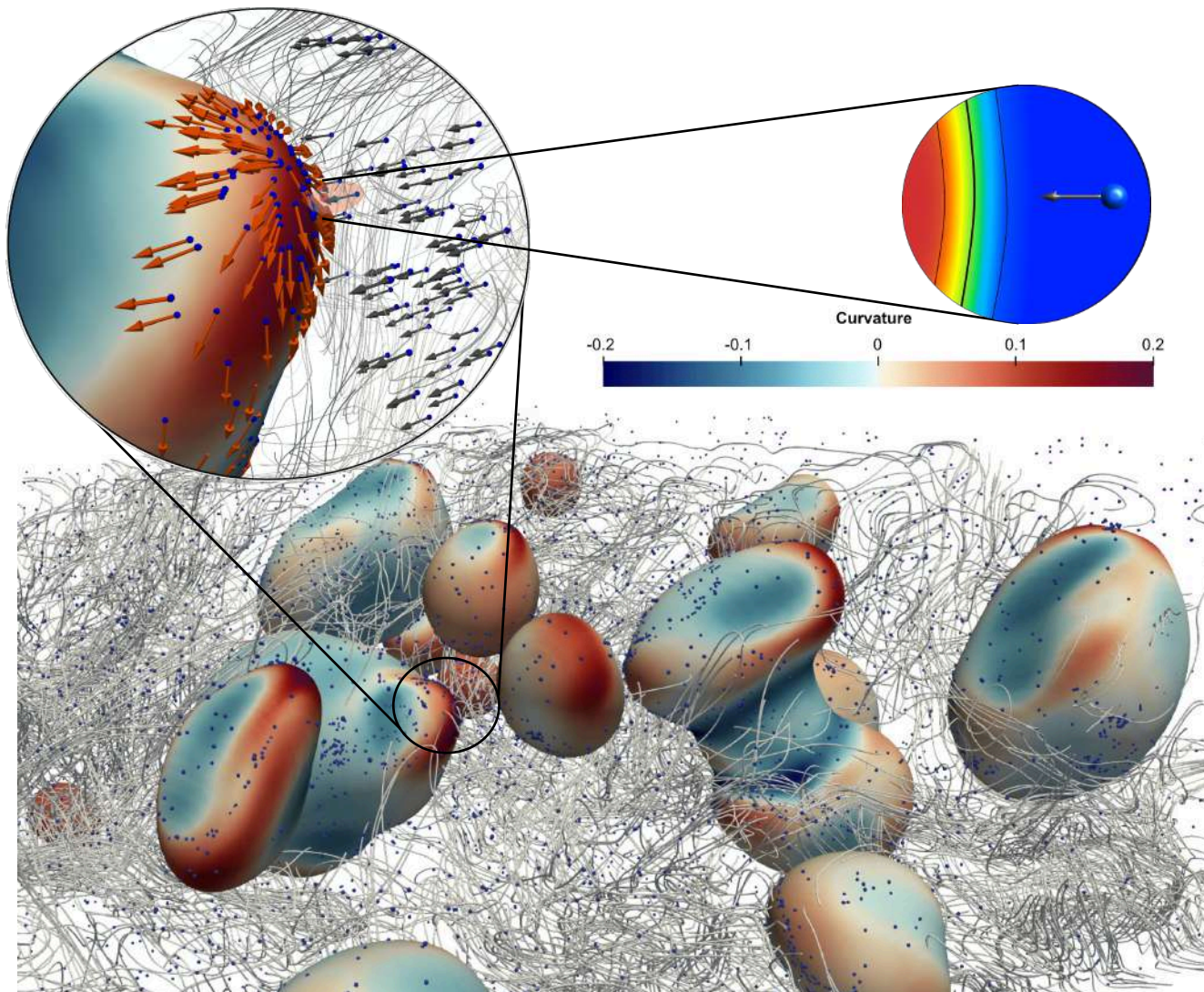


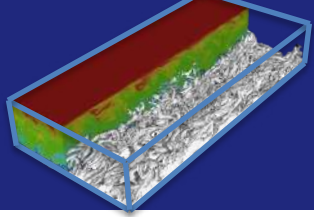
256 Droplets

10^6 Particles



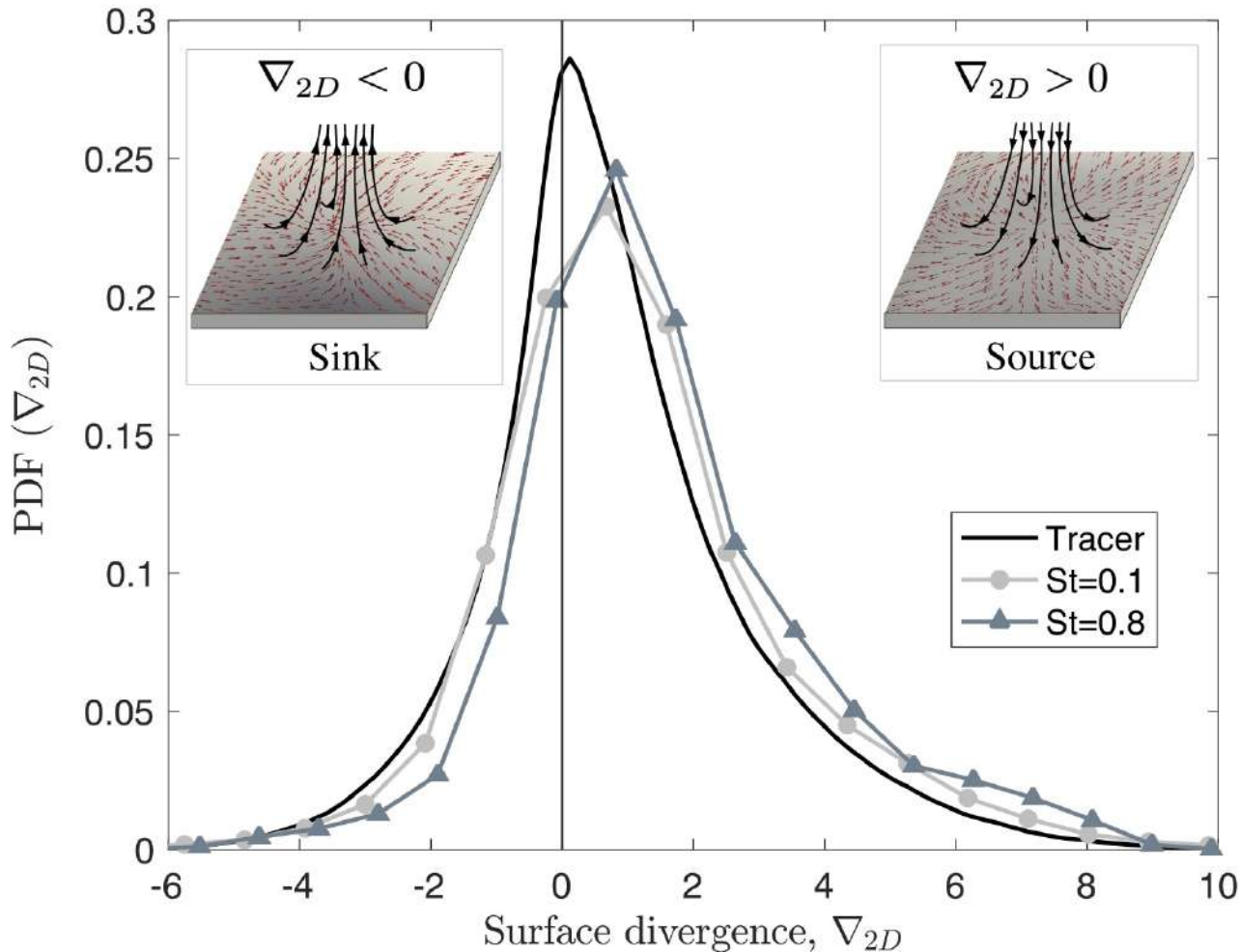
Particle capture at the drop interface

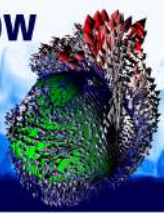
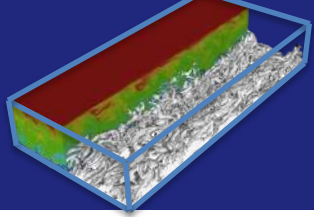




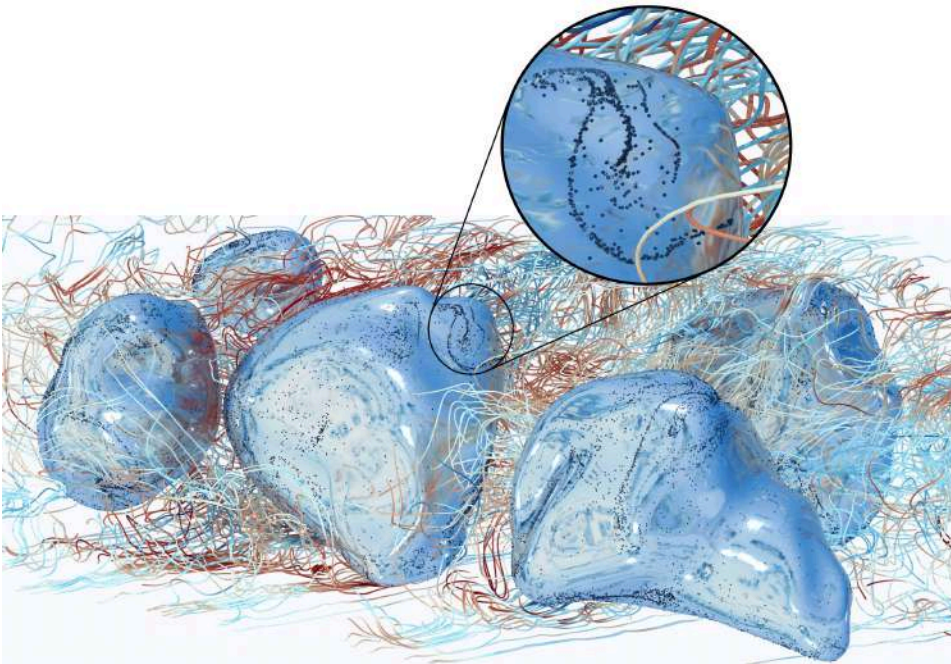
Particle capture at the drop interface

$$\nabla_{2D} = \mathbf{n} \cdot \nabla \times (\mathbf{n} \times \mathbf{u})$$

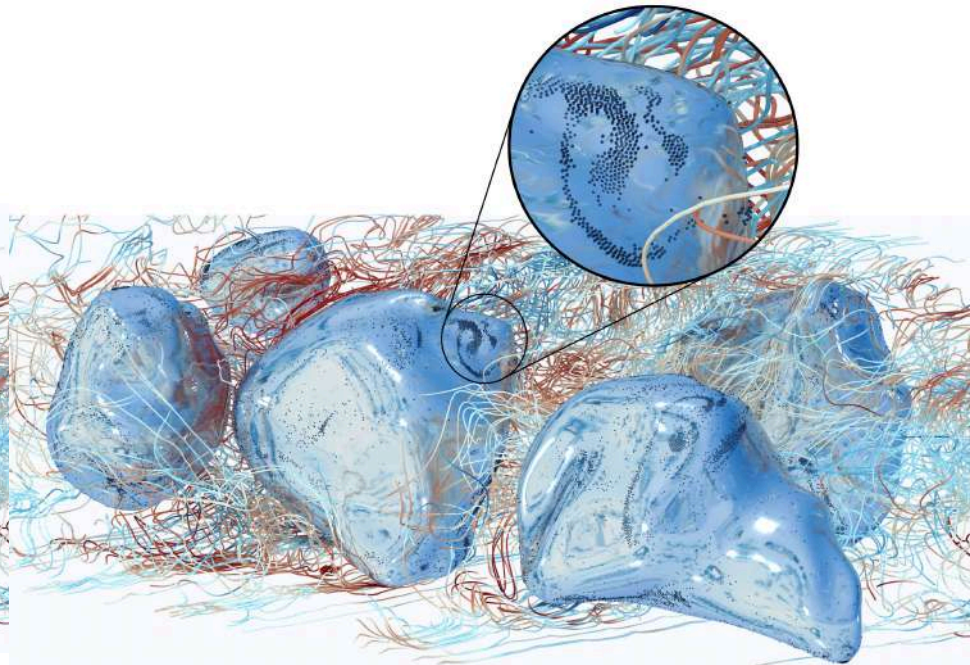




Particle trapping at the drop interface



Without Excluded-Volume Effects (EVE)



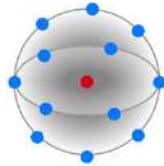
With Excluded-Volume Effects (EVE)

Excluded-Volume Effects (EVE) are accounted for via particle-particle collisions

Collision algorithm: hard-sphere proactive collisions (Sundaram & Collins, 1996)

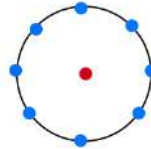
Particle trapping at the drop interface

Volumetric Distribution



correlation Dimension=3

Planar Distribution

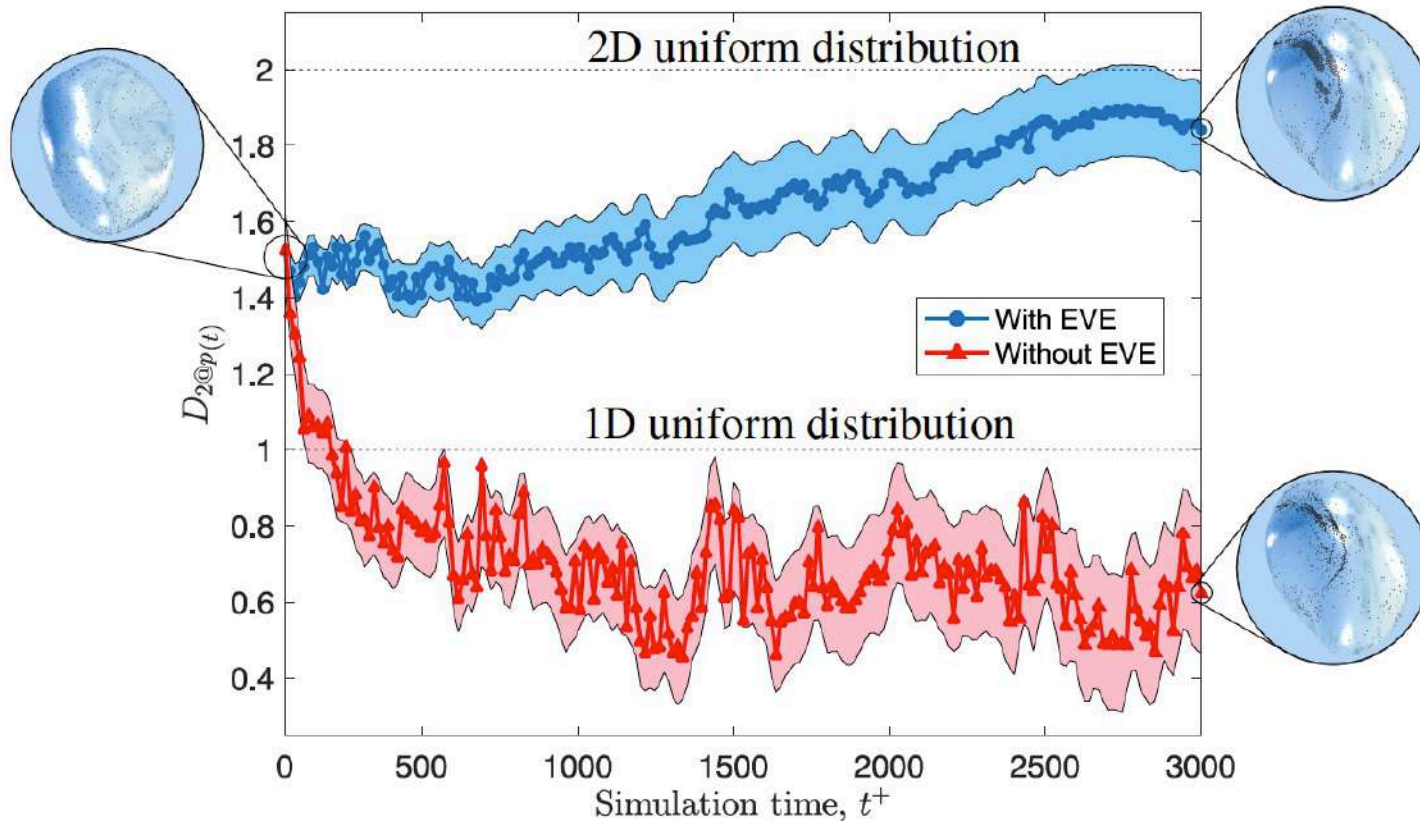


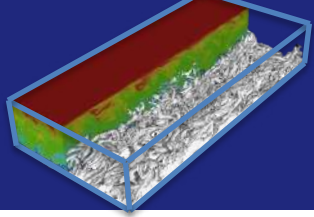
correlation Dimension=2

Linear Distribution



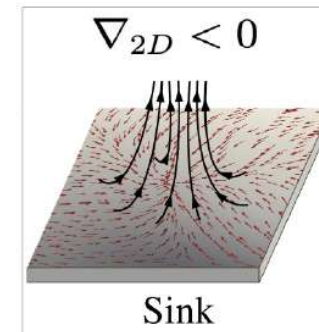
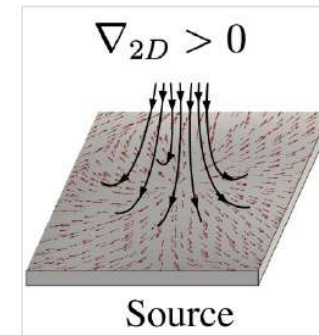
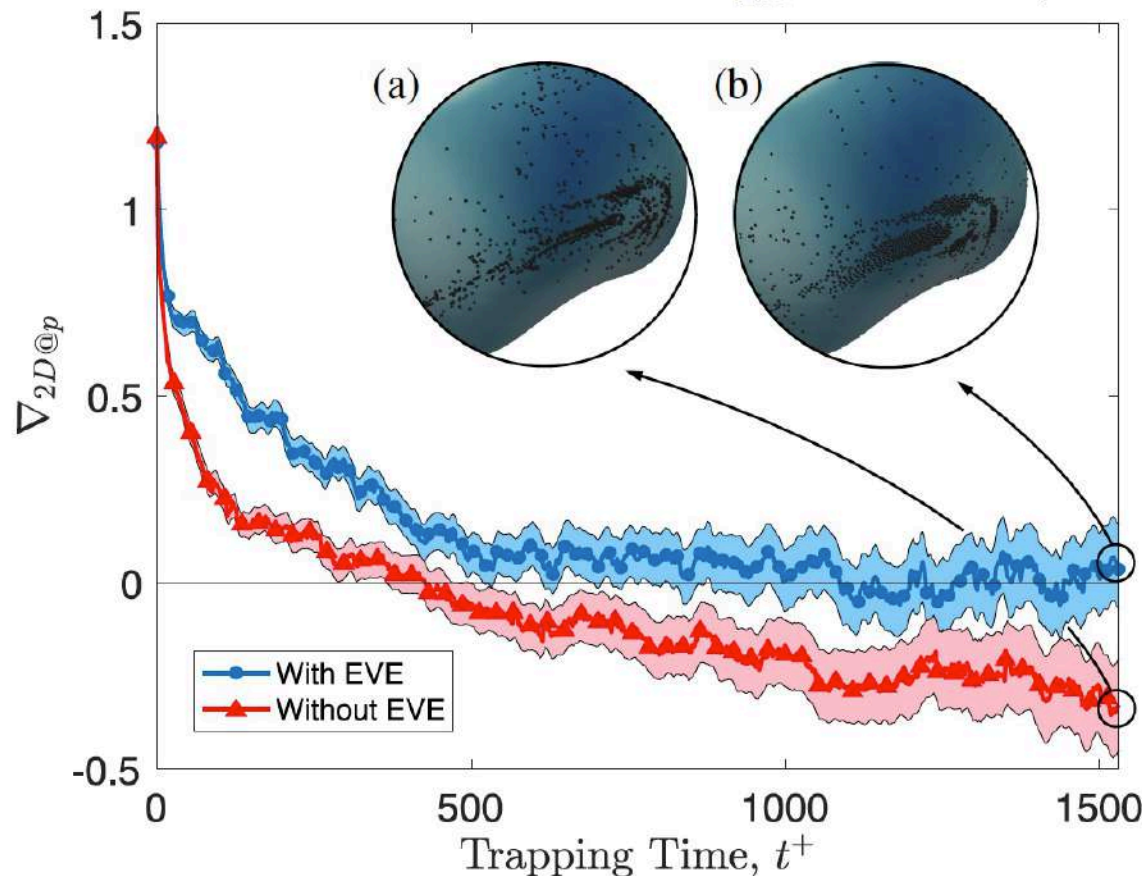
correlation Dimension=1





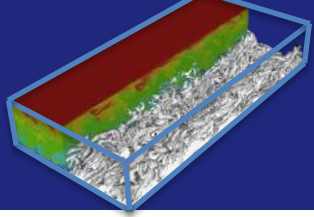
Particle trapping at the drop interface

$$\nabla_{2D} = \mathbf{n} \cdot \nabla \times (\mathbf{n} \times \mathbf{u})$$



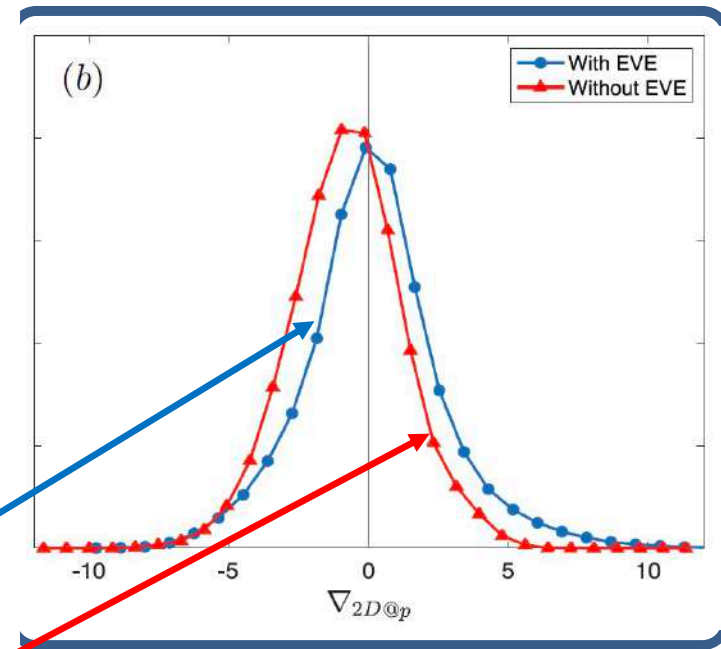
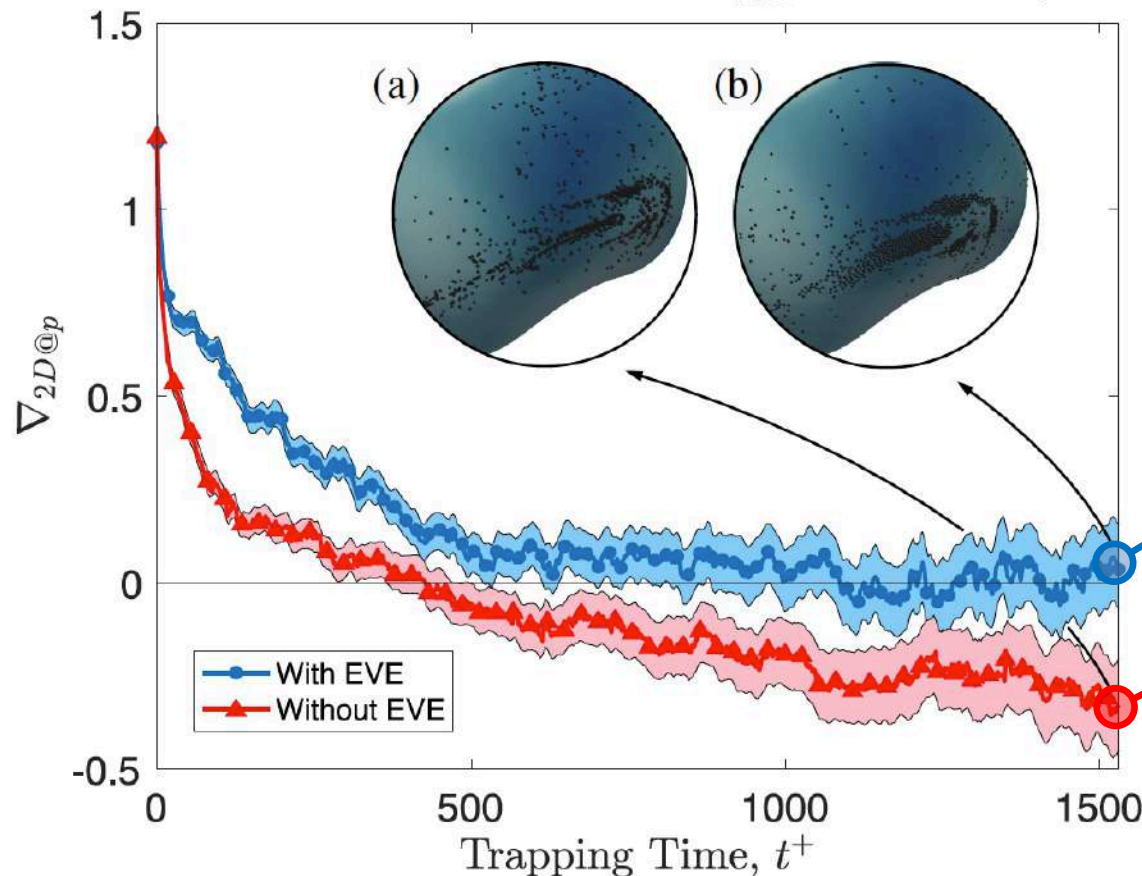
Shaded area:
 $\chi(t) = \nabla_{2D@p}(We, St, t) - \nabla_{2D@p}(0.75, 0.1, t)$

Profiles refer to $We=0.75$, $St=0.1$



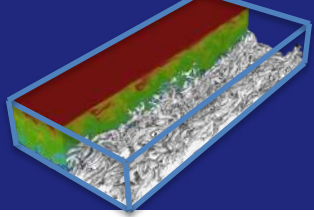
Particle trapping at the drop interface

$$\nabla_{2D} = \mathbf{n} \cdot \nabla \times (\mathbf{n} \times \mathbf{u})$$



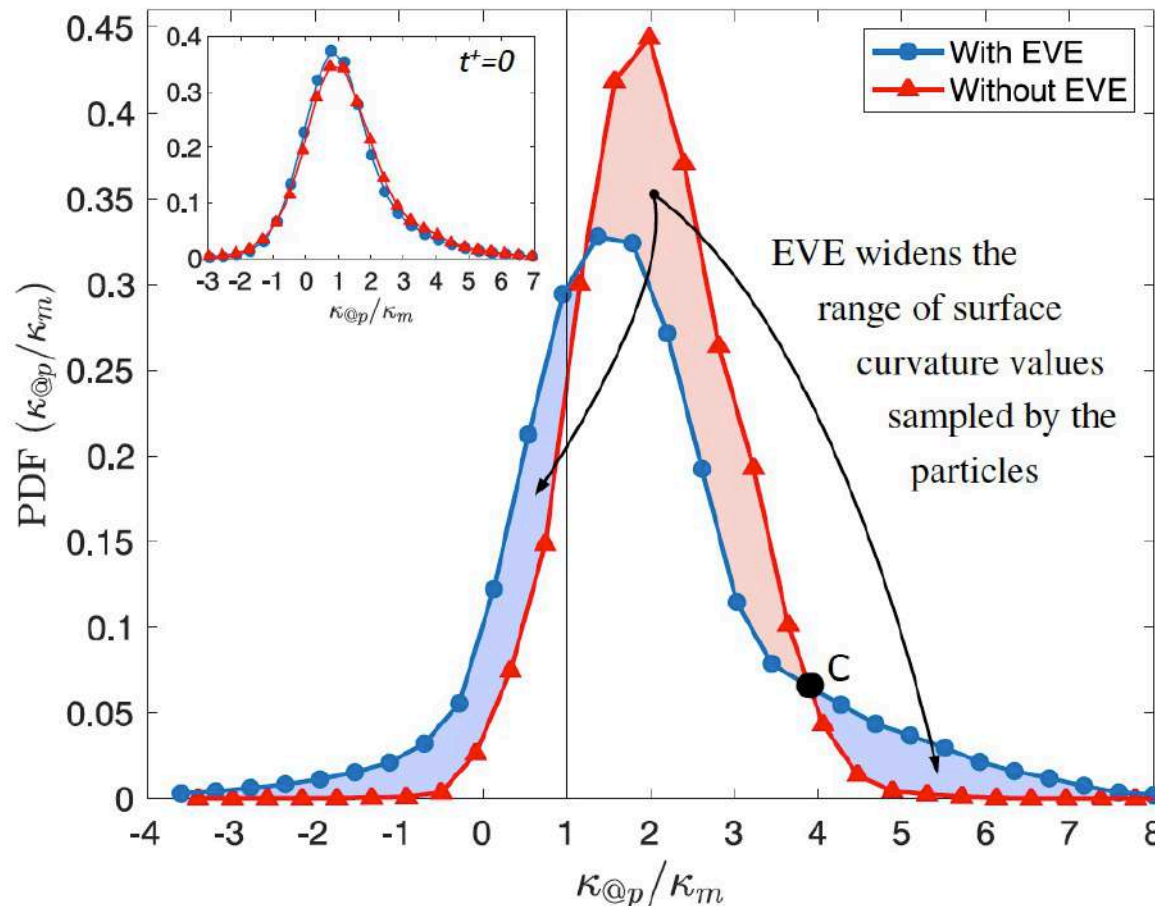
PDF of $\nabla_{2D}@p$ sampled at the position of the trapped particles at time $t^+=1500$ after capture

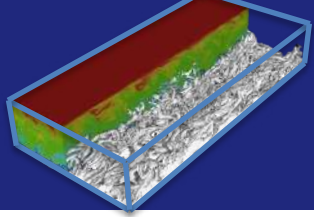
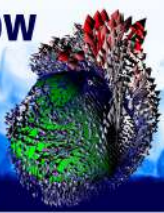
Shaded area:
 $\chi(t) = \nabla_{2D}@p(We, St, t) - \nabla_{2D}@p(0.75, 0.1, t)$



Particle trapping at the drop interface

$$\kappa = -\nabla \cdot \left(\frac{\nabla \phi}{|\nabla \phi|} \right) = -\frac{\nabla^2 \phi}{|\nabla \phi|} + \frac{1}{|\nabla \phi|^2} \nabla \phi \cdot \nabla (|\nabla \phi|)$$





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Thank you very much for your kind attention!

