

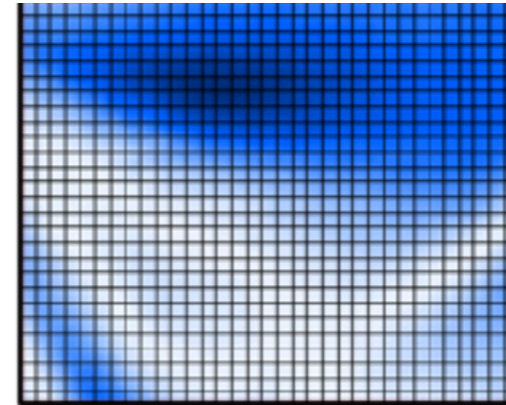
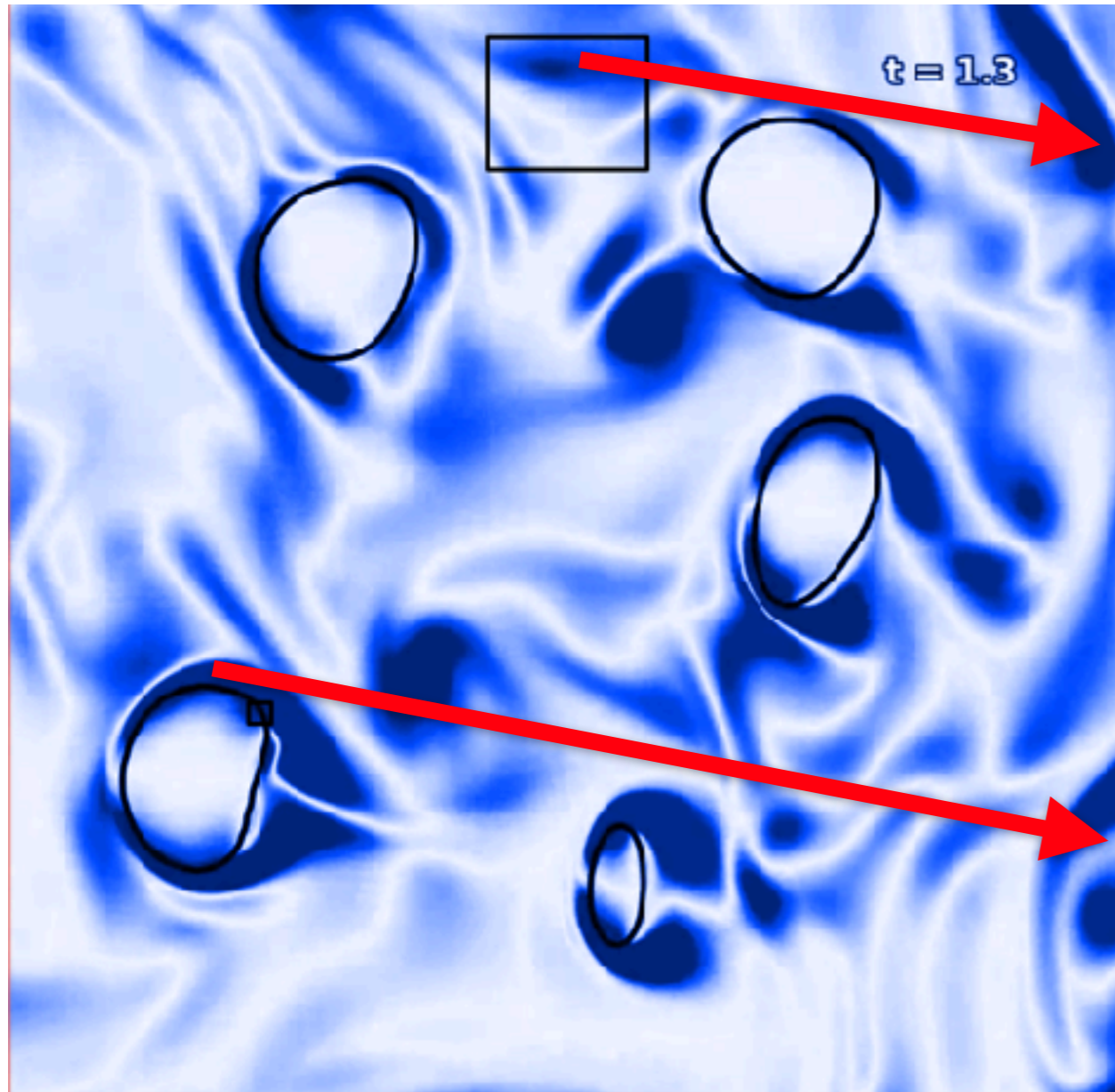
COMETE kickoff

Simulation of turbulent bubbly flows

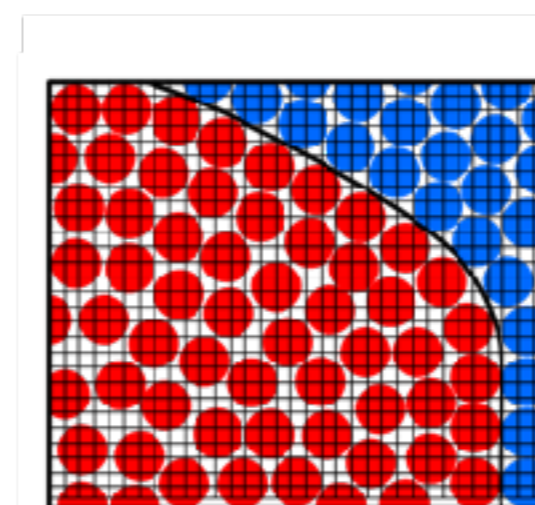
Gabriele Labanca



Homogeneous Isotropic Turbulence (HIT) in a cube of $1m^3$



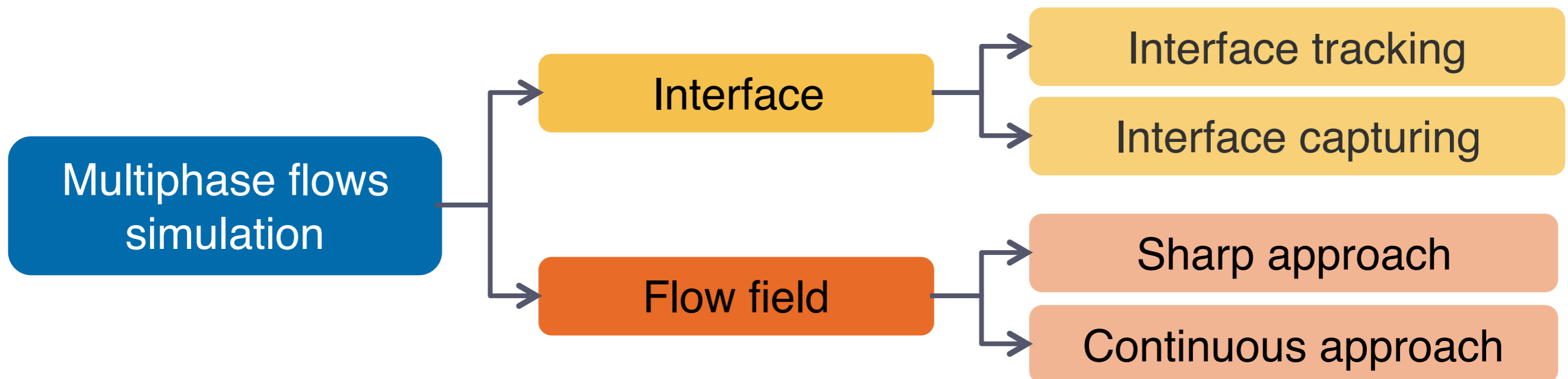
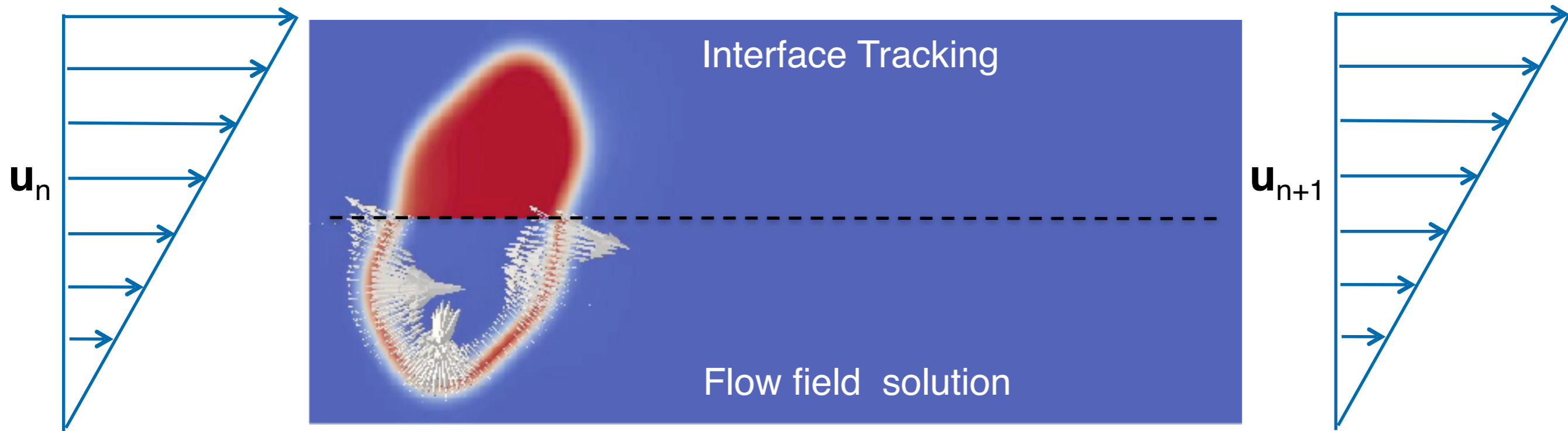
Turbulence:
 $Re_\lambda = 85$
 \Rightarrow smallest scale $\simeq 10^{-3}m$
3 orders of magnitude.



Interface:
 smallest Scale $\simeq 10^{-9}m$
 9 orders of magnitude.

$$N_P \simeq (10^9)^3 = 10^{27}!$$

Approaches to model the interface

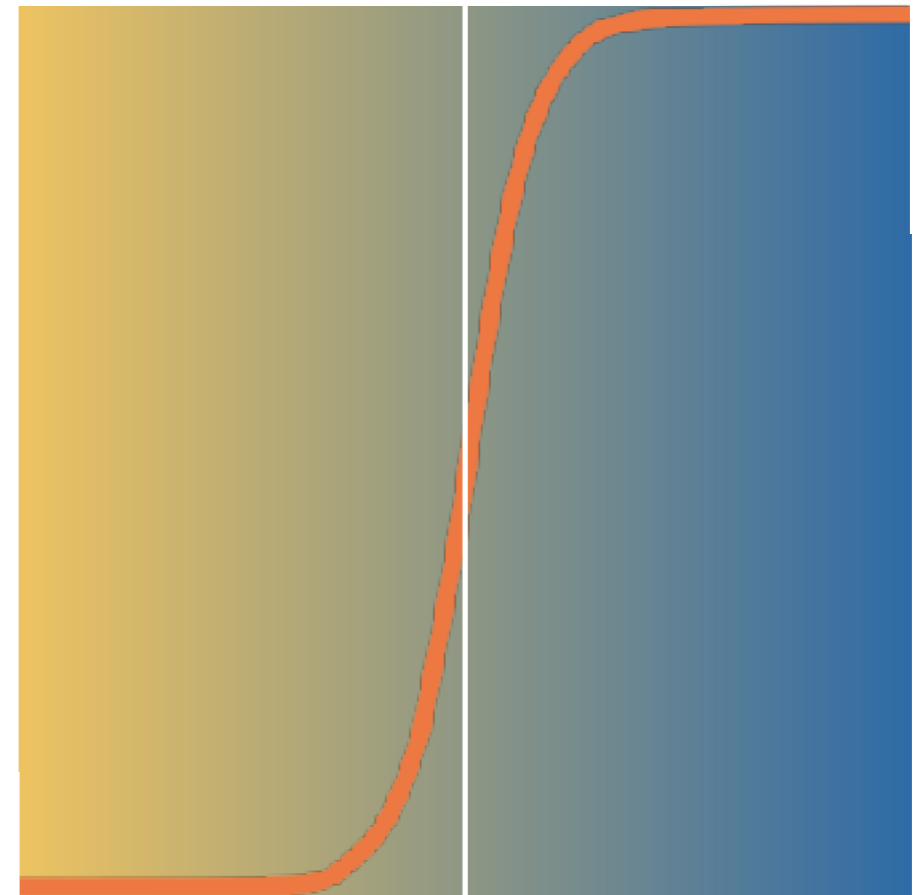


INTERFACE TRACKING



Interface described by points
Lagrangian advection

INTERFACE CAPTURING



Scalar function:
phase characterised by its value

Cahn-Hilliard Equation

$$\frac{\partial \phi}{\partial t} + \mathbf{u} \cdot \nabla \phi = \nabla \cdot \left(\mathcal{M}_\phi \nabla \mu_\phi \right) \quad \dots \rightarrow \quad \frac{\partial \phi}{\partial t} + \mathbf{u} \cdot \nabla \phi = \frac{1}{Pe_\phi} \nabla^2 \mu_\phi$$

Mobility parameter \mathcal{M}_ϕ

Advection by flow $\mathbf{u} \cdot \nabla \phi$

Diffusion by chemical potential $\frac{1}{Pe_\phi} \nabla^2 \mu_\phi$

Peclet number: ratio between diffusive and convective time scales

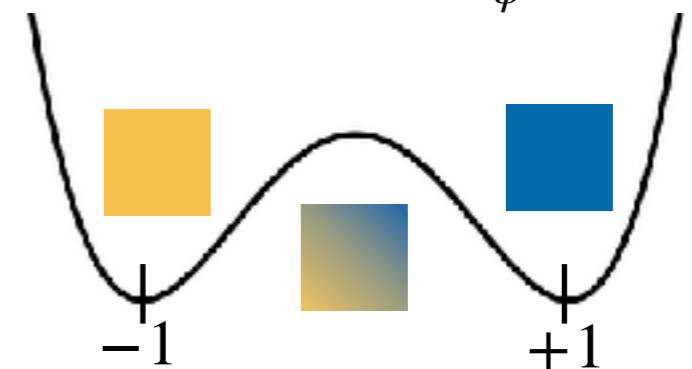
$$\mu_\phi = \frac{\delta \mathcal{F}[\phi, \nabla \phi]}{\delta \phi}$$

$$\mathcal{F}[\phi, \nabla \phi] = \int_{\Omega} [f_0(\phi) + f_i(\nabla \phi)] d\Omega$$

● $f_0(\phi) = \frac{1}{4}(\phi - 1)^2(\phi + 1)^2$ Phobic term

● $f_i(\nabla \phi) = \frac{Ch^2}{2} |\nabla \phi|^2$ Surface term

$$Pe_\phi = \frac{u_\tau h}{\mathcal{M}_\phi}$$



Cahn number: $Ch = \frac{\xi}{h}$

Unique equation for both fluids: properties depending on phase field value

Ratio of viscosities: $\lambda = \frac{\eta_d}{\eta_c}$

Width of the interface

$$\rho(\phi) \left[\frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} \right] = -\nabla \mathcal{P} + \frac{1}{Re_\tau} \nabla \cdot \left[\eta(\phi) \left(\nabla \mathbf{u} + \nabla \mathbf{u}^T \right) \right] + \frac{3}{\sqrt{8}} \frac{Ch}{We} \nabla \cdot \tau_c$$

Density dependent on phase field

Weber number: ratio of inertial over surface forces

$$We = \frac{\rho U^2 h}{\sigma}$$

Korteweg stress tensor: capillary force due to surface tension

$$\tau_c = \left| \nabla \phi \right|^2 \mathbf{I} - \nabla \phi \otimes \nabla \phi$$

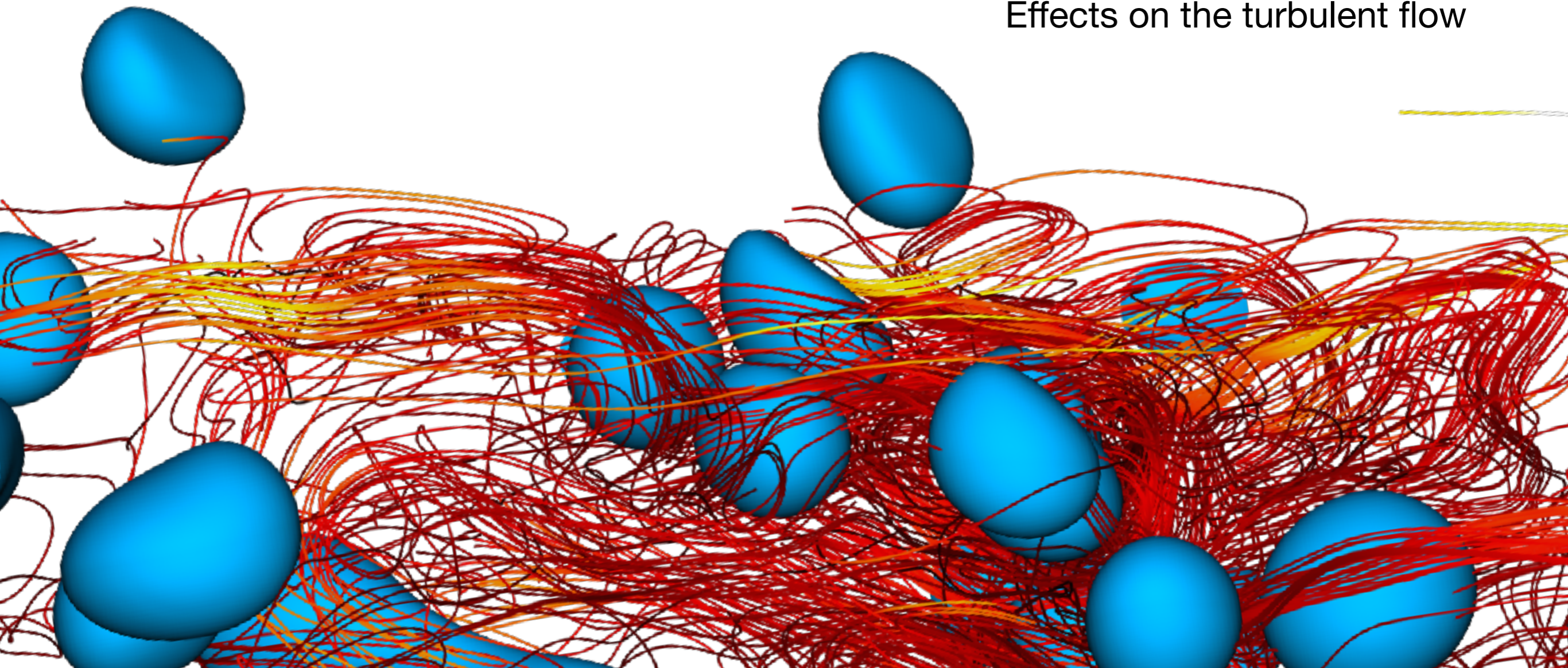
Different values of
viscosity and density ratios



Study of droplet-droplet interactions

Droplet statistics

Effects on the turbulent flow



Reynolds number: inertial over viscous

$$Re_\tau = \frac{\rho u_\tau h}{\eta_c}$$

Weber number: ratio between inertial and surface forces

$$We = \frac{\rho u_\tau^2 h}{\sigma}$$

Viscosity ratio: $\lambda = \frac{\eta_d}{\eta_c} = 0.01 \div 100$

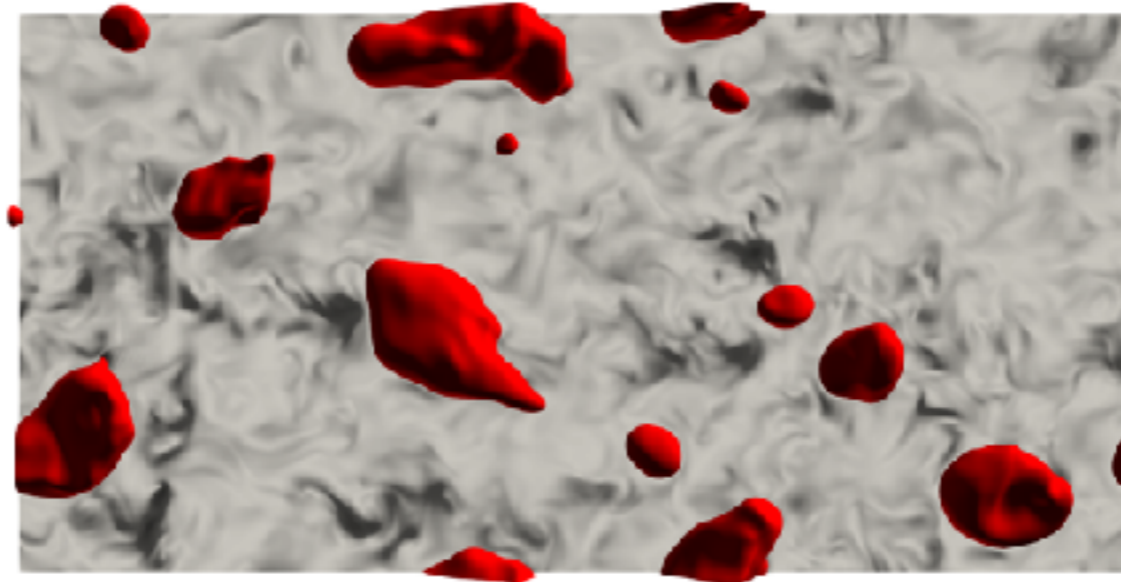
Density ratio: $\gamma = \frac{\rho_d}{\rho_c} = 0.001 \div 1$

		Viscosity ($Pa \cdot s$)		Density ($kg \cdot m^{-3}$)
Air		10^{-5}		1
Water		10^{-3}		10^3
Butane		10^{-5}		600
$\gamma \backslash \lambda$		0.01	1	100
	0.001			
	0.01			
	0.1			
	1			

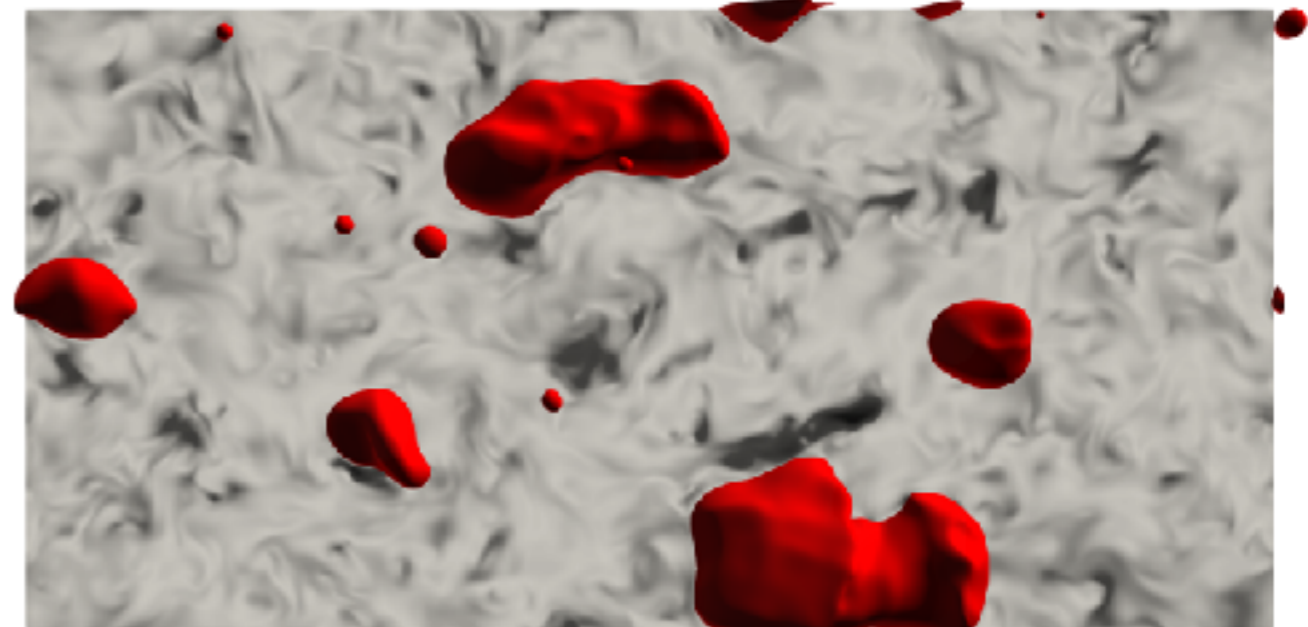
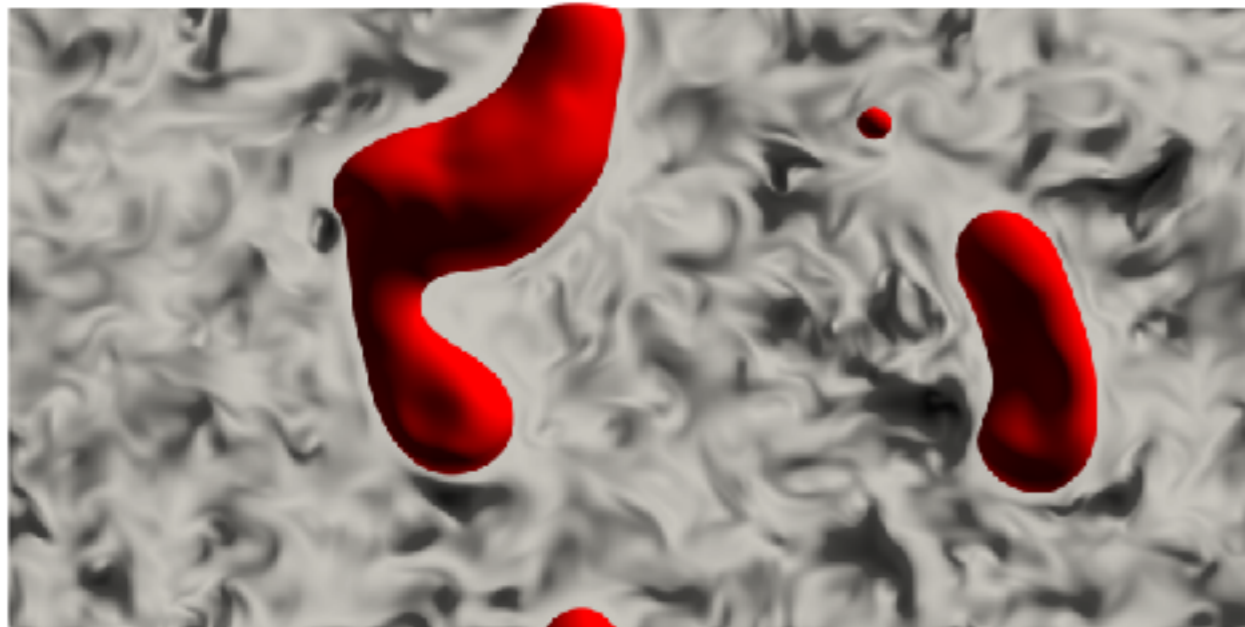
Results: qualitative differences

$$\lambda = \gamma = 1$$

Viscosity ratio $\lambda = 100$



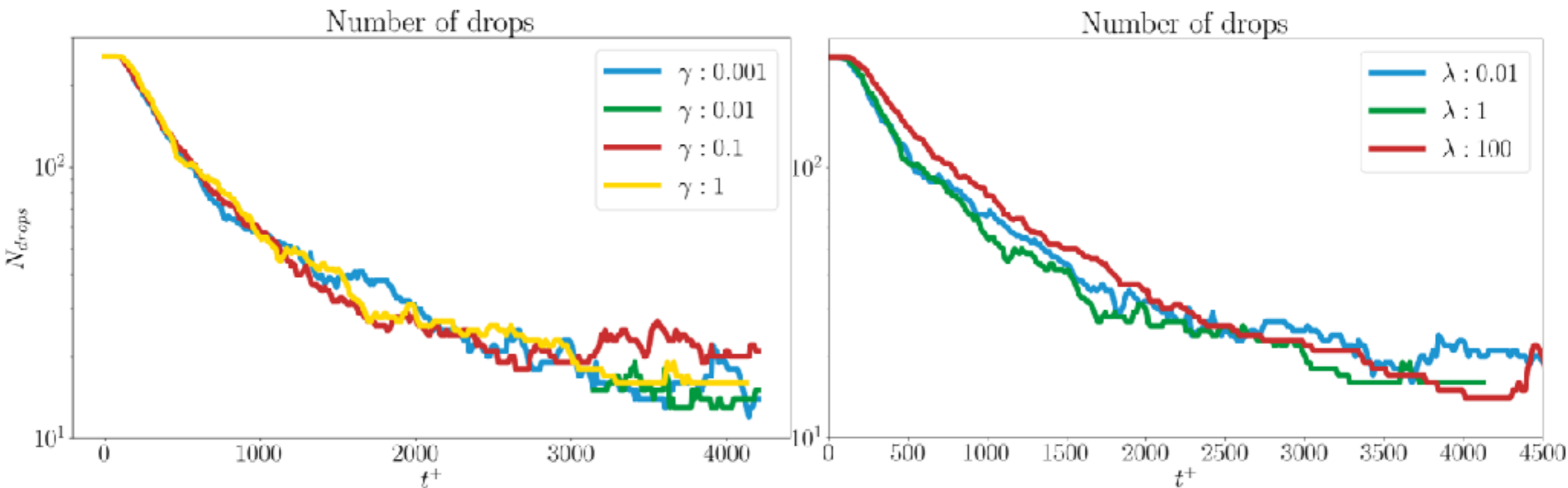
Density ratio $\gamma = 0.001$



Higher viscosity leads to drops more resistant to breakage



Dominance of coalescence events leads to a lower number of drops



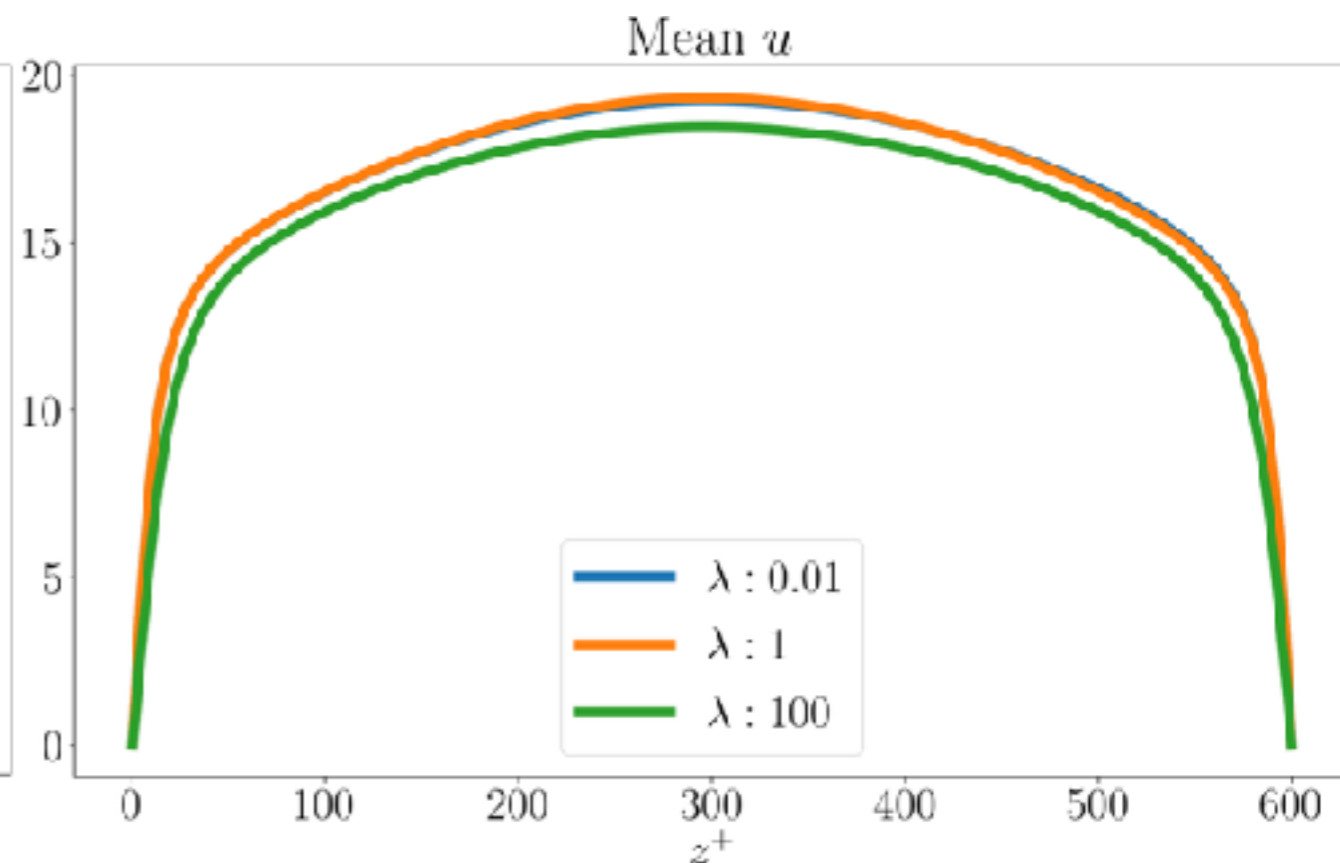
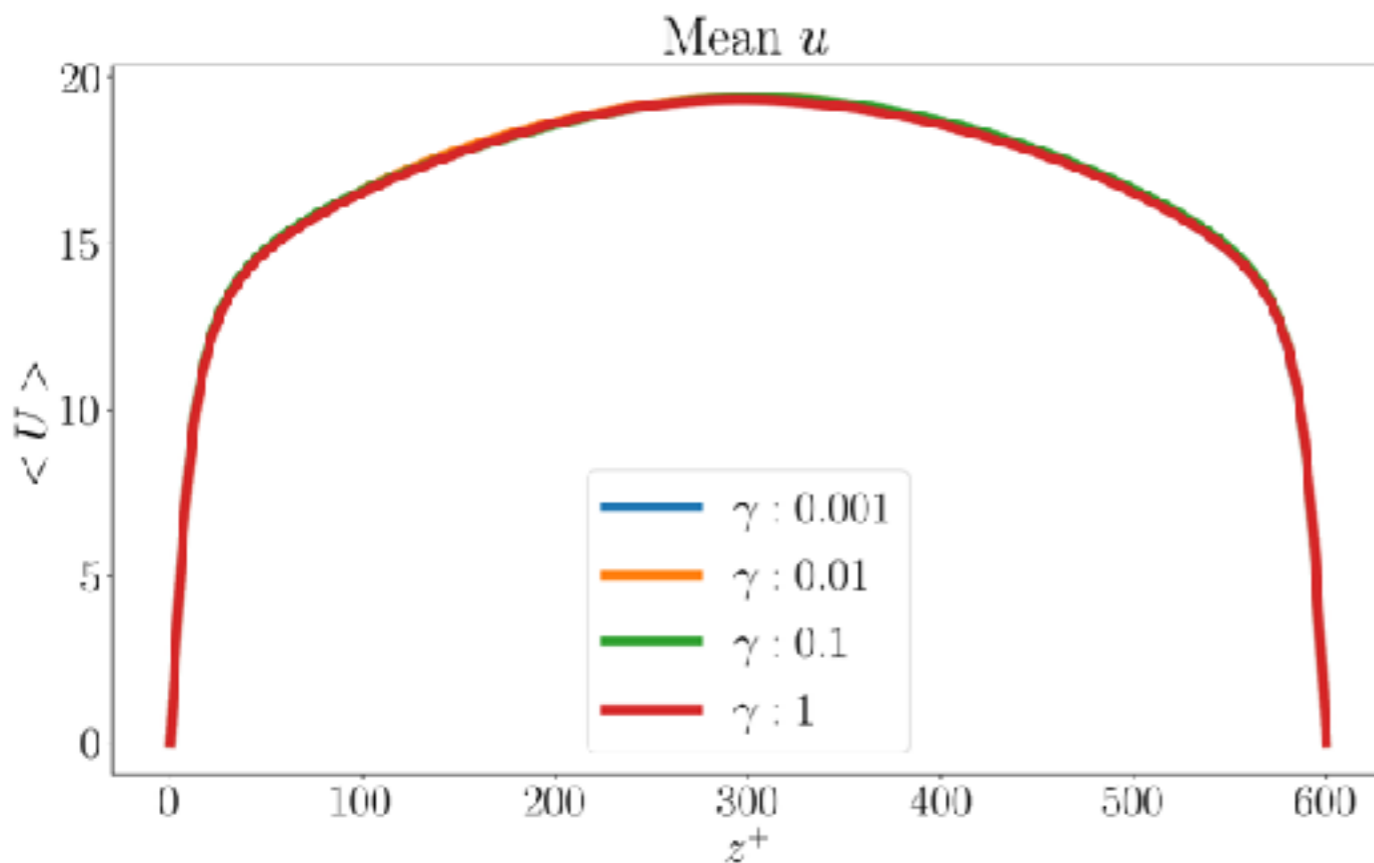
Results: Mean streamwise velocity

Streamwise component of velocity averaged over streamwise (\hat{x}) and span wise (\hat{y}) directions

Resistance to deformation damps the flow

No significant changes for different γ

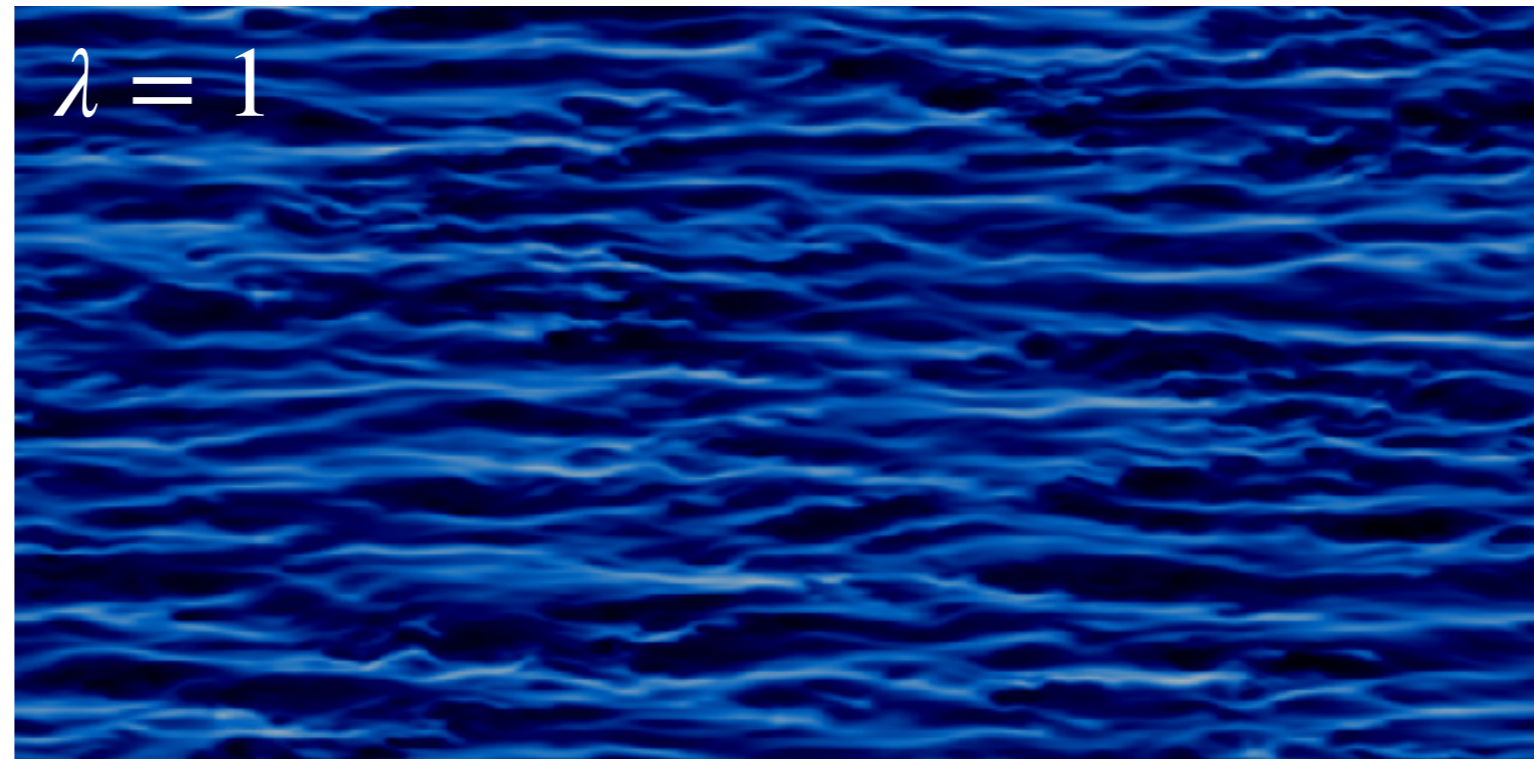
Global reduction for $\lambda = 100$



$\mathbf{u}' \cdot \mathbf{u}'$ evaluated at
10 w.u. from the wall



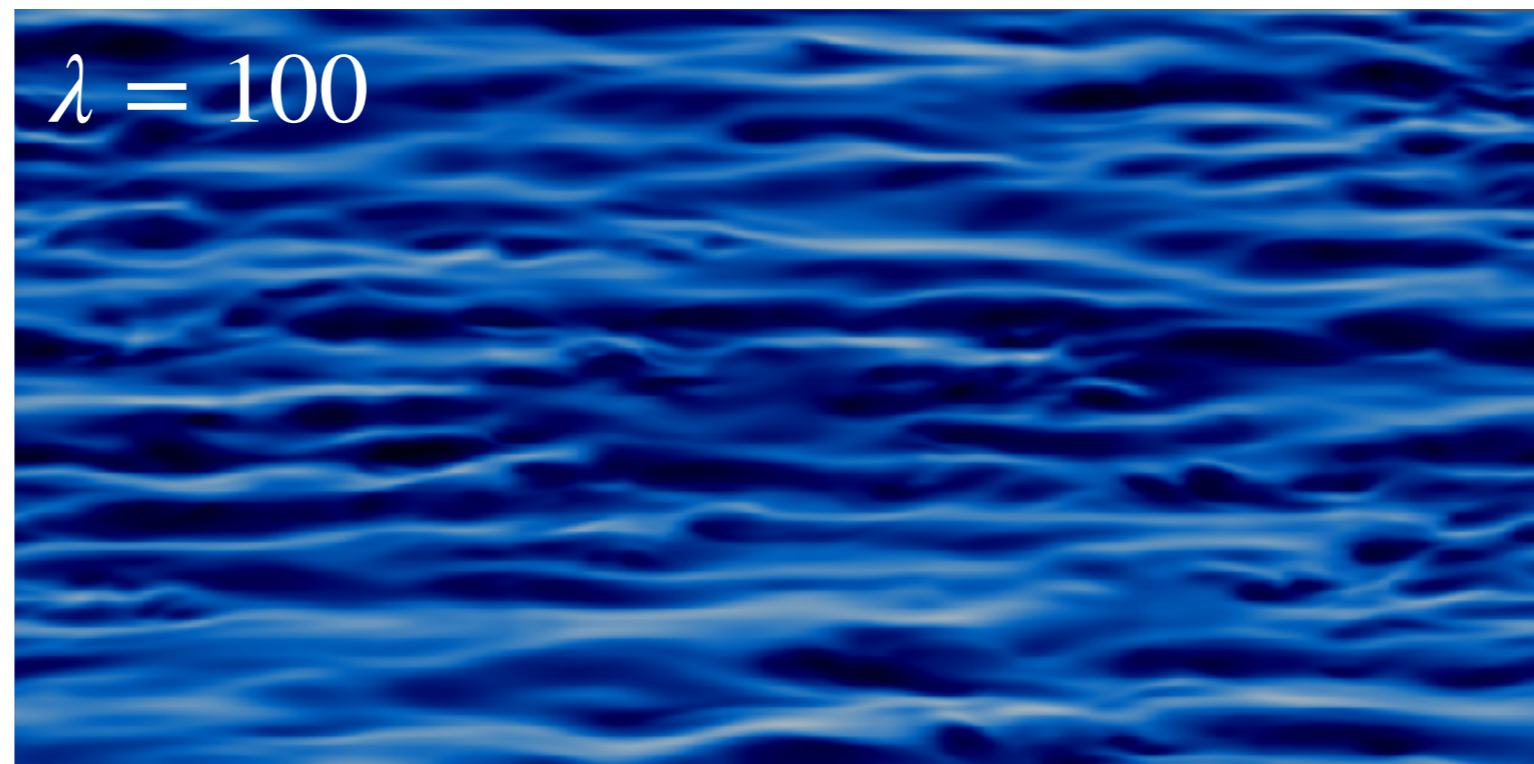
Structures aligned
with streamflow



At higher λ , the bubbles
resist more to deformations



Less streaks, bigger timescales
Globally, higher fluctuations



Continuation of the analysis

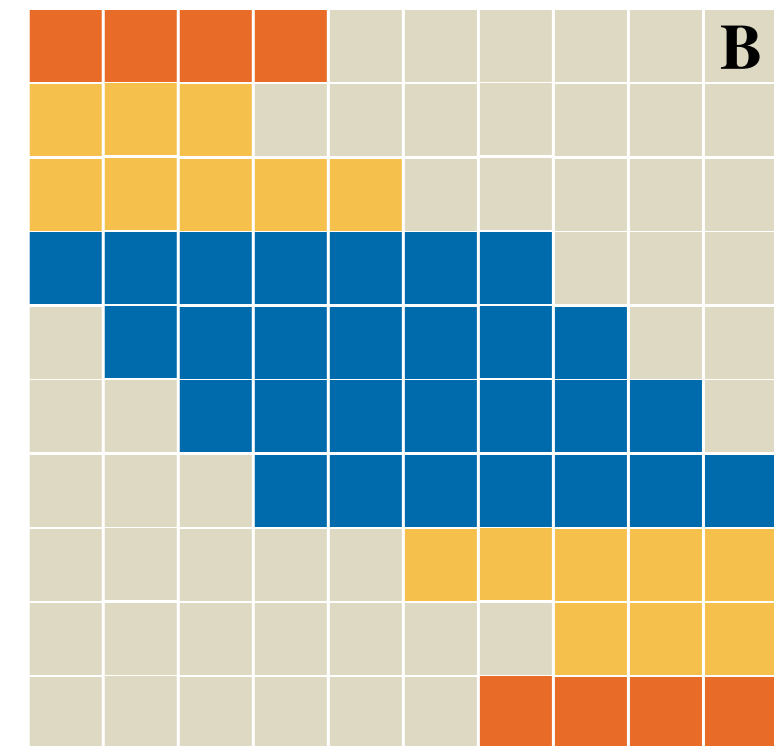
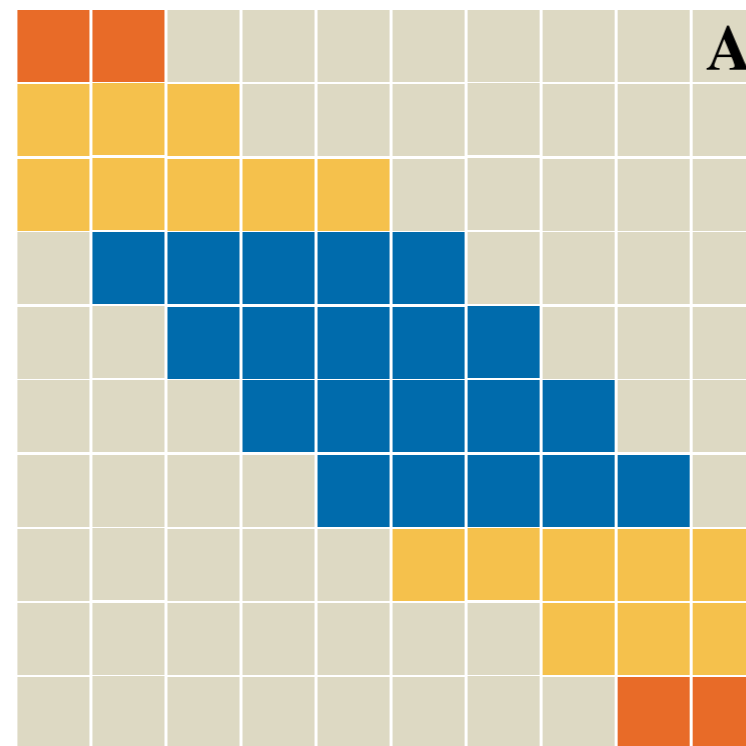
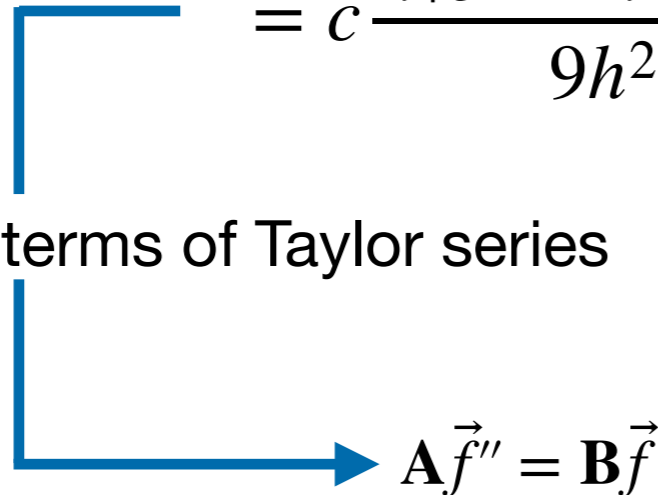
Widening of the range of parameters (FD wall-normal direction)

Conferences: ERCOFTAC, APS (november 2019)

Uniform grid

$$= c \frac{\beta f''_{i-2} + \alpha f''_{i-1} + f''_i + \alpha f''_{i+1} + \beta f''_{i+2}}{9h^2} + b \frac{f_{i+2} - 2f_i + f_{i-2}}{4h^2} + a \frac{f_{i+1} - 2f_i + f_{i-1}}{h^2}$$

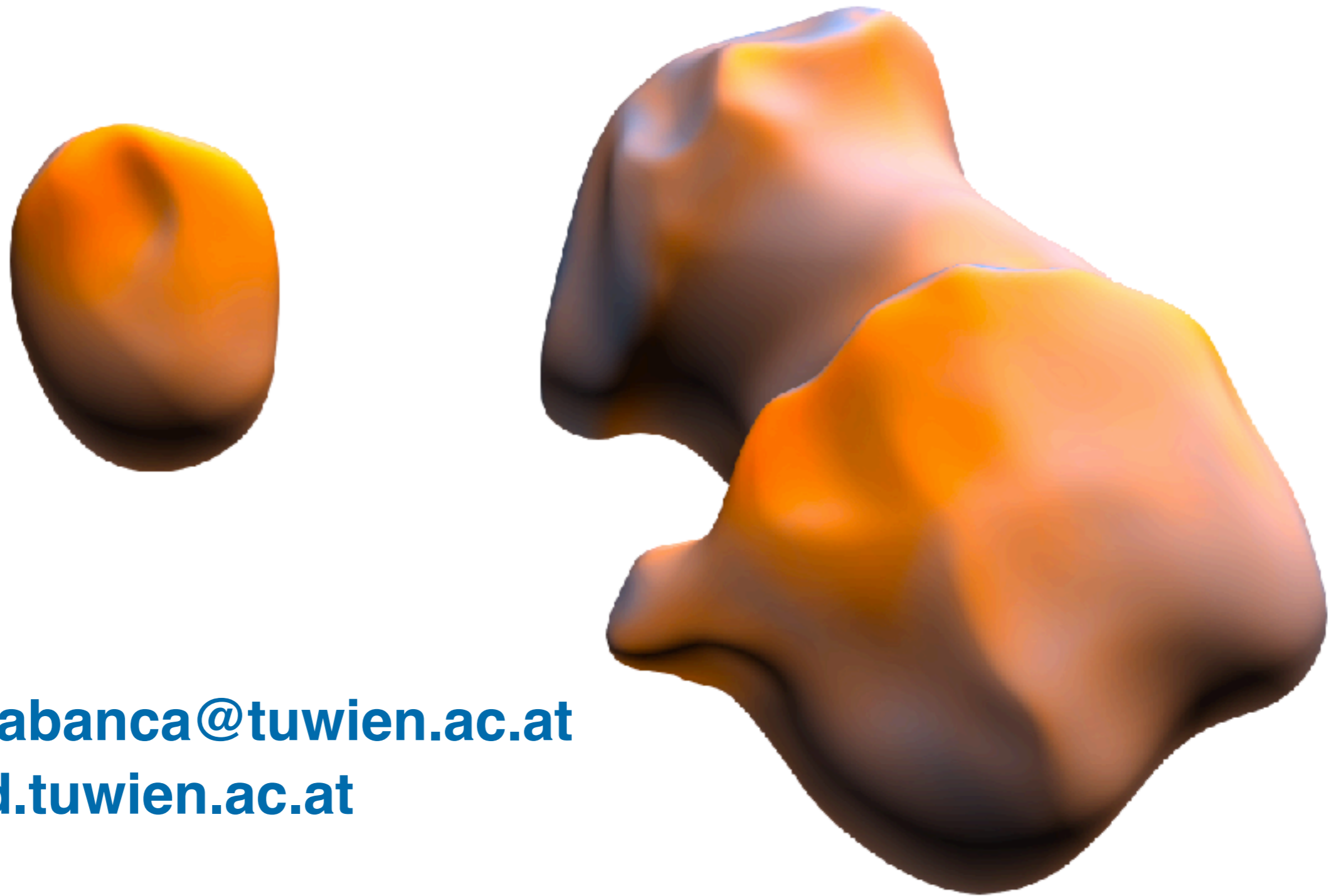
Matching terms of Taylor series



Non-uniform grid

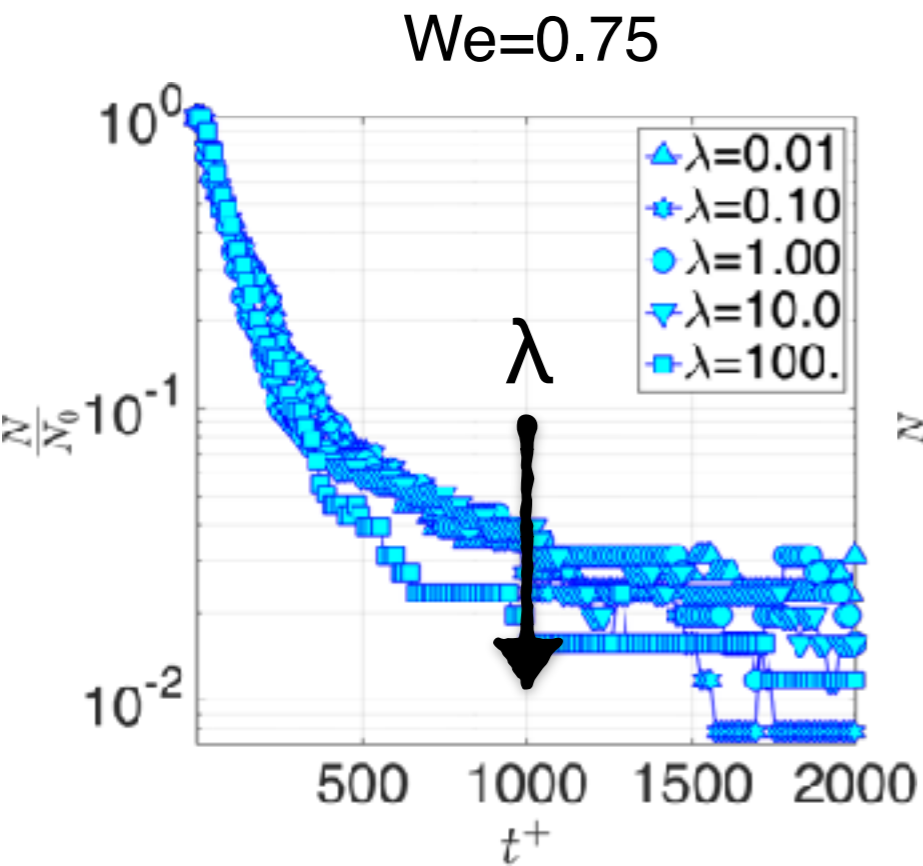
General compact finite difference scheme: $u_i^{(p)} + \sum_{j \in J_n} a_j u_j^{(p)} = \sum_{j \in I_n} b_j u_j + \sum_{j \in J_m} b_j u_j$

The coefficients can be derived with polynomial interpolation and adapted to non-uniform grid (Chebyshev)

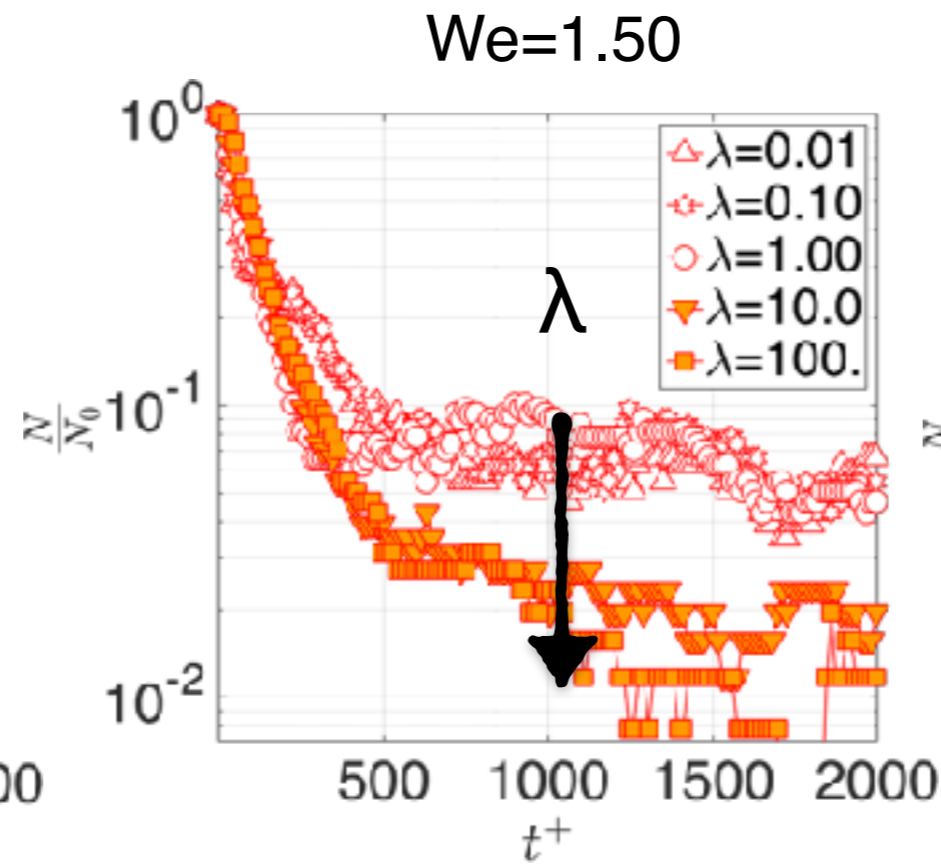


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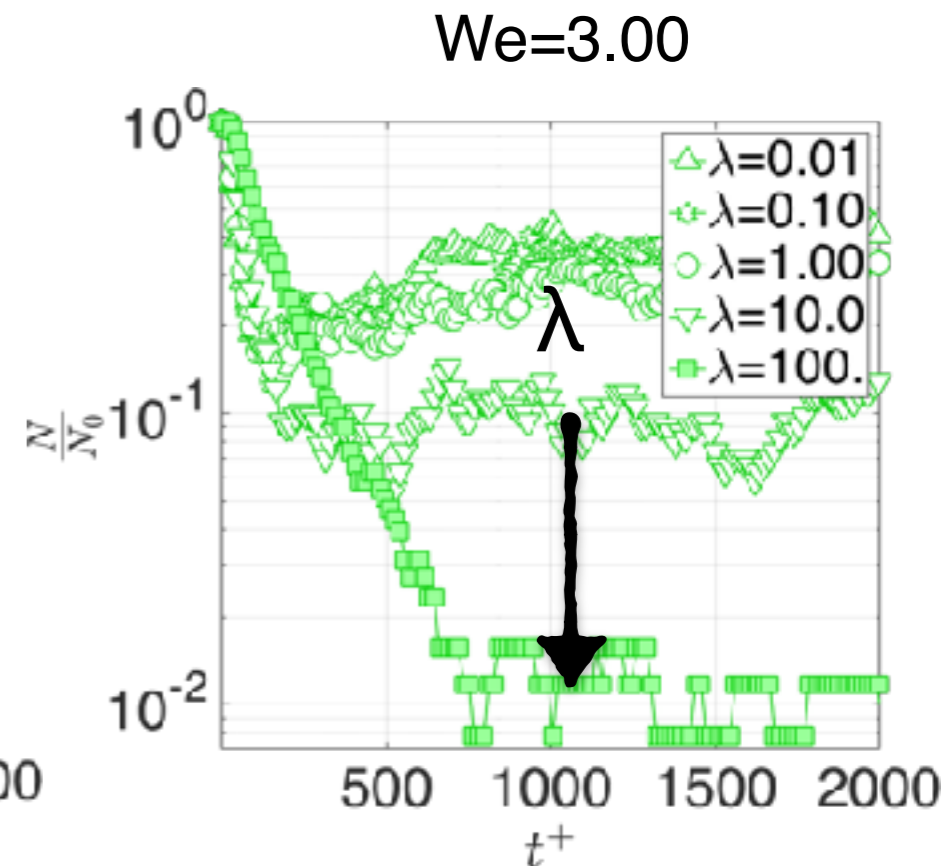
Collision/Coalescence/Break-up Drops & Carrier Fluid w. different viscosity



Coalescence Regime for every λ

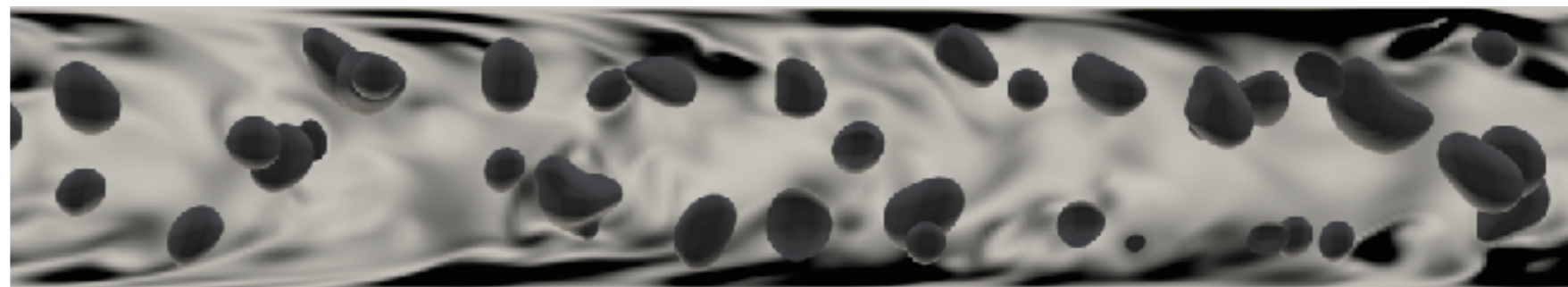


Coalescence Regime for $\lambda < 1$
Break-up Regime for $\lambda > 1$



Coalescence Regime for $\lambda < 1$
Break-up Regime for $\lambda > 1$

$$\lambda = \frac{\eta_d}{\eta_c} = \frac{\text{Drop Viscosity}}{\text{Continuous Viscosity}}$$



L. Scarbolo, A. Soldati et. al., Unified framework for a side-by-side comparison of different multicomponent algorithms, JCP. (2013)

A. Roccon, M. De Paoli, F. Zonta, A. Soldati, Viscosity-modulated breakup and coalescence of large drops in bounded turbulence, PRF (2017)

$$\frac{\partial \psi}{\partial t} + \mathbf{u} \cdot \nabla \psi = \nabla \cdot \left[\psi(1 - \psi) \nabla \mu_\psi \right] \quad \mu_\phi = \frac{\delta \mathcal{F}[\phi, \nabla \phi, \psi]}{\delta \phi} \quad \mu_\psi = \frac{\delta \mathcal{F}[\phi, \nabla \phi, \psi]}{\delta \psi}$$

$$\mathcal{F}[\phi, \nabla \phi, \psi] = \int_{\Omega} \left[f_0(\phi) + f_i(\nabla \phi) + f_\psi(\psi) + f_1(\phi, \psi) + f_b(\phi, \psi) \right] d\Omega$$

● $f_\psi(\psi) = Pi \left[\psi \log \psi + (1 - \psi) \log(1 - \psi) \right]$ Entropy term Pi : diffusivity

● $f_1(\phi, \psi) = -\frac{1}{2} \psi (1 - \phi^2)^2$ Adsorption term

● $f_b(\phi, \psi) = \frac{1}{2E_x} \phi^2 \psi$ Solubility term E_x : solubility

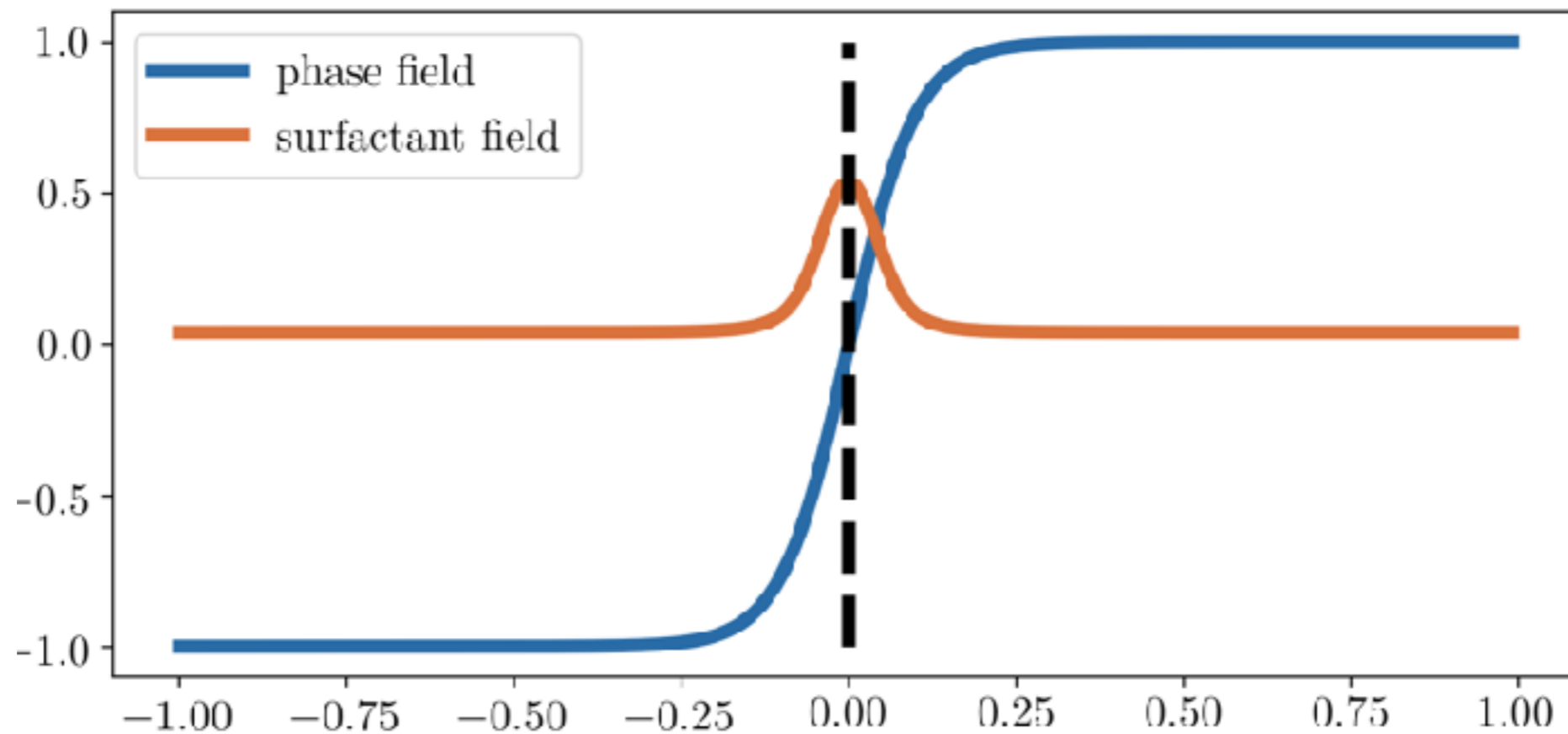
$$\frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} = -\nabla \mathcal{P} + \frac{1}{Re_\tau} \nabla \cdot \left[\frac{(\lambda - 1)(\phi + 1)}{2} \left(\nabla \mathbf{u} + \nabla \mathbf{u}^T \right) \right] + \frac{3}{\sqrt{8}} \frac{Ch}{We} \nabla \cdot \left[\frac{\sigma(\psi)}{\sigma_0} \tau_c \right]$$

Variable surface tension \uparrow

$$\phi(x) = \tanh\left(\frac{x}{\sqrt{2}Ch}\right)$$

$$\psi(x) = \frac{\psi_{bulk}}{\psi_{bulk} + \psi_c(\phi)(1 - \psi_{bulk})}$$

$$\psi_c(\phi) = \exp\left[-\frac{1 - \phi^2}{2Pi} \left(1 - \phi^2 + \frac{1}{E_x}\right)\right]$$



● Reliability

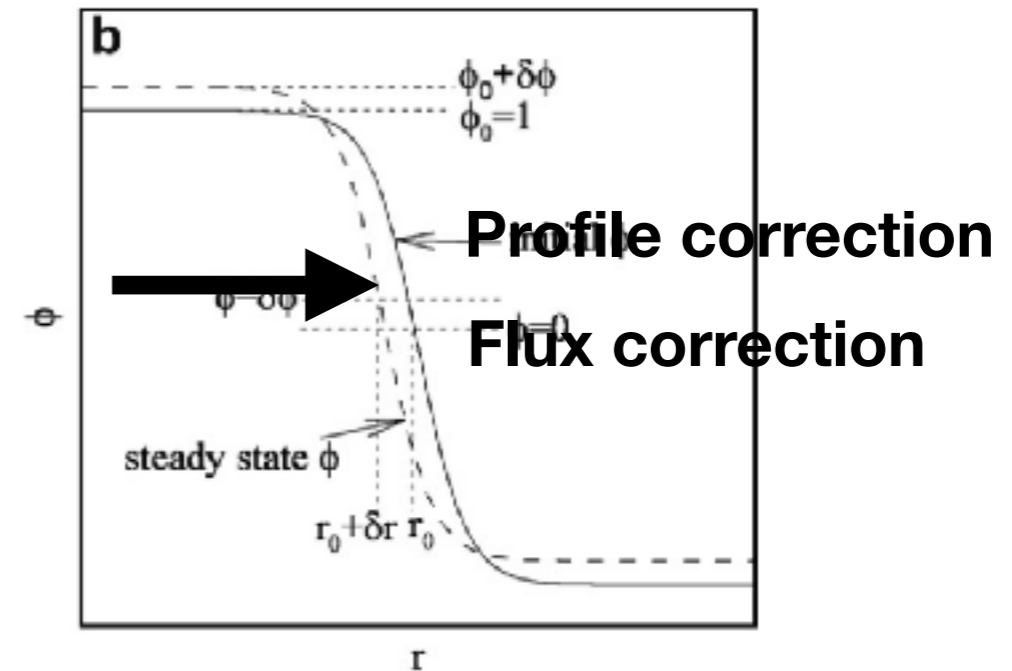
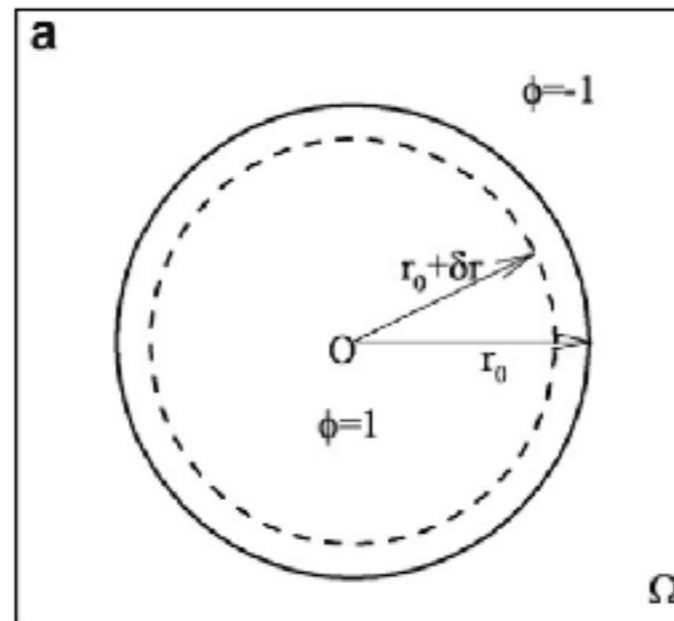
Spontaneous shrinkage of droplets

$$\frac{d\mathcal{F}}{dt} \leq 0$$

Total energy is lowered by drop shrinkage

$$\delta\mathcal{F} \propto \delta r$$

$$|\phi| > 1!$$



$$= c \frac{\beta f''_{i-2} + \alpha f''_{i-1} + f''_i + \alpha f''_{i+1} + \beta f''_{i+2}}{9h^2} + b \frac{f_{i+2} - 2f_i + f_{i-2}}{4h^2} + a \frac{f_{i+1} - 2f_i + f_{i-1}}{h^2}$$

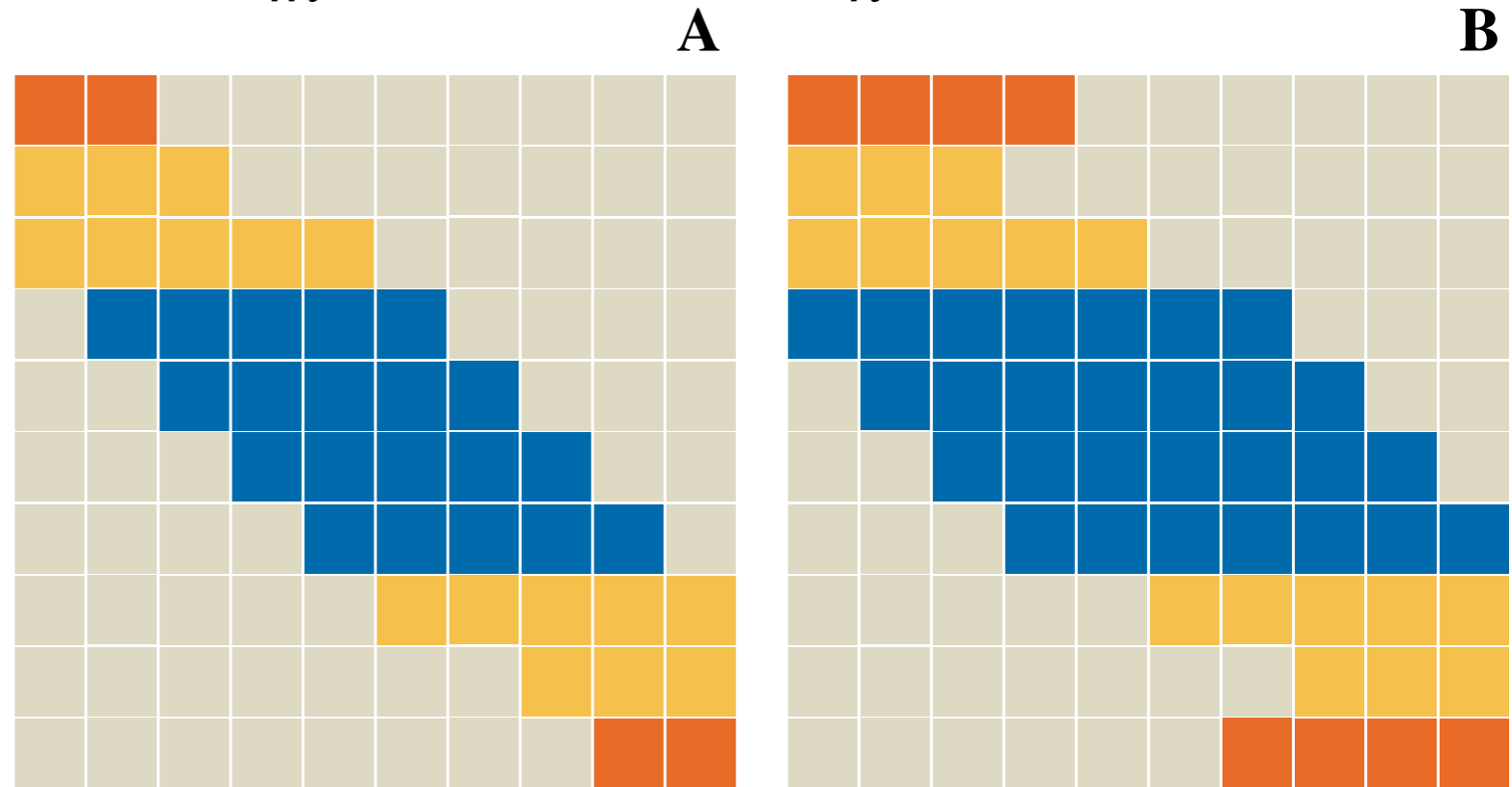
Matching terms of Taylor series



α, β, a, b, c



$$\mathbf{A} \vec{f}'' = \mathbf{B} \vec{f}$$



Helmholtz Equation: $P(x)f''(x) + Q(x)f(x) = R(x) \longrightarrow \vec{P} \cdot \vec{f}'' + \vec{Q} \cdot \vec{f} = \vec{R}$

$$\underbrace{(\vec{P} \cdot \mathbf{A}^{-1} \mathbf{B} + \vec{Q})}_{\vec{M}} \cdot \vec{f} = \vec{K}$$

General compact finite difference scheme: $u_i^{(p)} + \sum_{j \in J_n} a_j u_j^{(p)} = \sum_{j \in I_n} b_j u_j + \sum_{j \in J_m} b_j u_j$

$$u(x) = \sum_{i \in I_n} u_i \rho_i(x) + \sum_{i \in I_n} u_i'' q_i(x) + \sum_{i \in I_m} u_i r_i(x)$$

Conditions on ρ_i, q_i, r_i

$$\begin{aligned} \rho_i(x_j) &= \delta_{ij} \quad \forall i \in I_n, \forall j \in I_n \cup I_m \\ \rho_i''(x_j) &= 0 \quad \forall i \in I_n, \forall j \in I_n \end{aligned}$$

Guess of the form

$$\rho_i(x) = \frac{\prod_m(x)}{\prod_m(x_i)} l_i^n(x) \left(1 + \sum_{r=1}^n A_r (x - x_i)^r \right), \quad i \in I_n$$

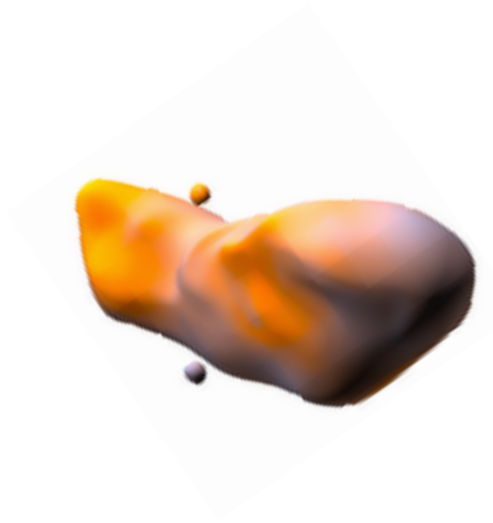
Differentiating and using the condition gives n equations in n unknowns A_1, A_2, \dots, A_n

The coefficients can be adapted to non-uniform grid (Chebyshev)



END

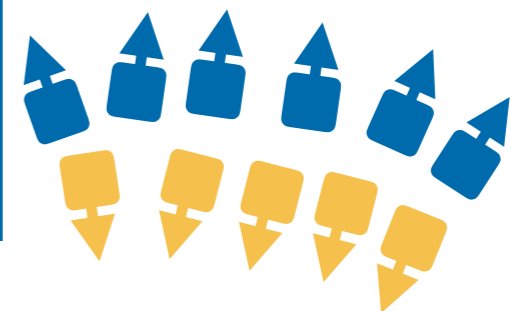
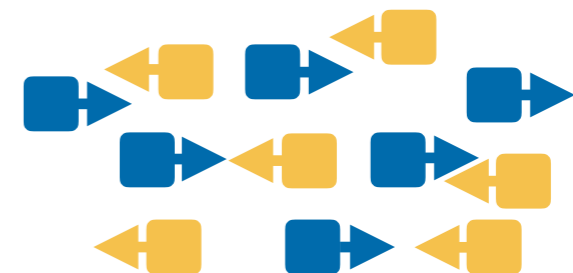
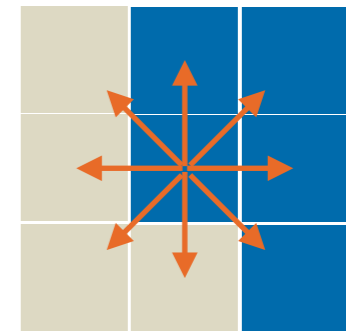




$$\left. \frac{\partial(\delta\mathcal{F})}{\partial(\delta r)} \right|_{\delta r=0} > 0$$

Advanced courses
Cross-topic training
Innovative methods

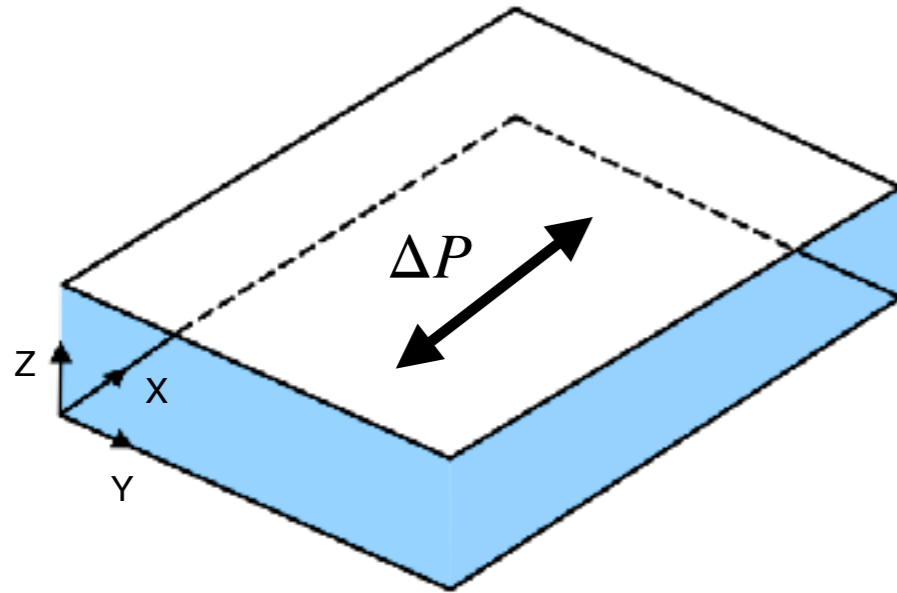
Drops are identified with the
flood fill algorithm



Implementation and testing of finite-differences method

Direct Numerical Solution (DNS) coupled CH and NS equations, no models used.

Computational Domain



Solver NS (Vorticity-Velocity Formulation)

Curl of NS (Vorticity):

$$\frac{d\omega}{dt} = \nabla \times \mathbf{S} + \frac{1}{Re_\tau} \nabla^2 \omega$$

Double Curl of NS (Vorticity)

$$\frac{d\nabla^2 \mathbf{u}}{dt} = \nabla^2 \mathbf{S} - \nabla(\nabla \cdot \mathbf{S}) + \frac{1}{Re_\tau} \nabla^4 \mathbf{u}$$

CH (Same formulation)

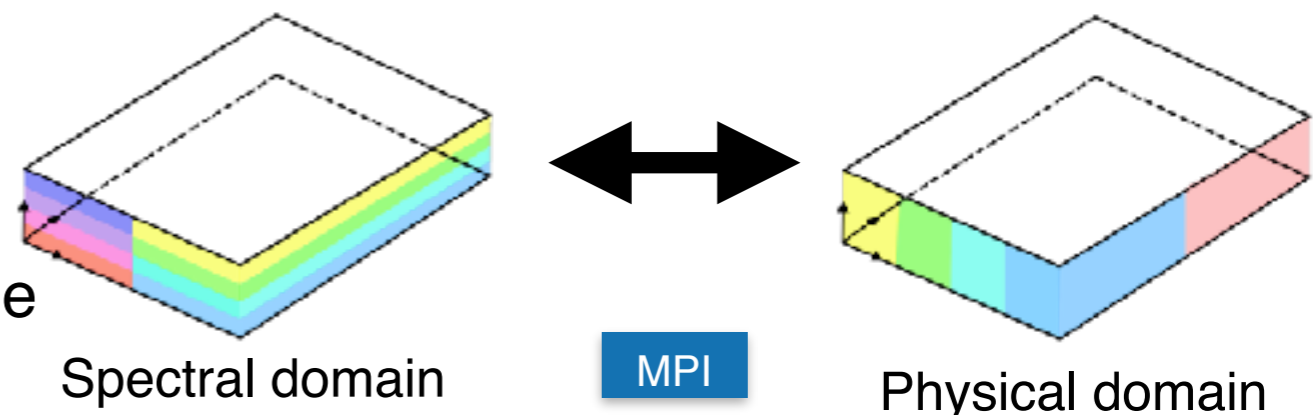
$$\frac{d\phi}{dt} = S_\phi + \frac{sCh^2}{Pe} \nabla^2 \phi - \frac{Ch^2}{Pe} \nabla^4 \phi$$

Space Discretisation:

- X Periodic direction (Fourier)
- Y Periodic direction (Fourier)
- Z Wall-normal (Chebyshev-Tau)

Time Discretisation:

- N-S: Crank-Nicolson/Adams-Bashforth scheme
- C-H: Crank-Nicolson/Euler scheme



TECHNICAL

- **Reliability**

- **Scaling**

- **Realistic parameters**

- **Publications**

- **Ease of use ↔ ESTECO**

COMMUNICATION

- **Conferences**